

## REMOVAL OF METHYL RED FROM AQUEOUS SOLUTION BY ACTIVATED CARBON PREPARED FROM THE *Annona squamosa* SEED BY ADSORPTION

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**Abstract:** The use of low-cost, locally available, highly efficient and eco-friendly adsorbents has been investigated as an ideal alternative to the current expensive methods of removing dyes from wastewater. This study investigates the potential use of activated carbon prepared from the *Annona squamosa* seed for the removal of methyl red (MR) dye from simulated wastewater. The effects of different system variables, adsorbent dosage, initial dye concentration, pH and contact time were investigated and optimal experimental conditions were ascertained. The results showed that as the amount of the adsorbent increased, the percentage of dye removal increased accordingly. Optimum pH value for dye adsorption was 4.0. Maximum dye was sequestered within 50 min of the start of every experiment. The adsorption of methyl red followed the pseudo-second-order rate equation and fits the Langmuir, Freundlich, Dubinin-Radushkevich (D-R) and Tempkin equations well. The maximum removal of MR was obtained at pH 4 as 82.81% for adsorbent dose of 0.2 g/ 50 mL and 25 mg L<sup>-1</sup> initial dye concentration at room temperature. Furthermore, adsorption kinetics of MR was studied and the rate of adsorption was found to conform to pseudo-second-order kinetics with a good correlation ( $R^2 > 0.99$ ) with intraparticle diffusion as one of the rate determining steps. Activated carbon developed from the *Annona squamosa* seed can be an attractive option for dye removal from diluted industrial effluents since test reaction made on simulated dyeing wastewater showed better removal percentage of MR.

**Keywords:** *Annona squamosa*, Adsorption, Wastewater, Methyl red, Kinetics, Activated carbon

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### 1. Introduction

Industrial effluents are one of the major causes of environmental pollution because effluents discharged from dyeing industries are highly colored with a large amount of suspended organic solid [1]. Untreated disposal of this colored water into the receiving water body either causes damage to aquatic life or to human beings by mutagenic and carcinogenic effect. As a matter of fact, the discharge of such effluents is worrying for both toxicological and environmental reasons [2, 3].

Conventional wastewater treatment methods for removing dyes include physicochemical, chemical and biological methods, such as coagulation and flocculation [4], adsorption [5], ozonation [6], electrochemical techniques [7], and fungal decolonization [8]. Among these methods adsorption has gained favour in recent years due to proven efficiency in the removal of pollutants from effluents. Activated carbon, as an adsorbent has been widely investigated for the adsorption of dyes [9], but its high cost limits its commercial application. In recent years, there has been growing interest in finding inexpensive and effective alternatives to carbon, such as rice husk [10], chitin [11], orange waste [12], lemon peel [13], granular kohlrabi peel [14], raw barley straw [15], eggshell [16], *Ricinus communis* [17].

*Annona squamosa* is a commonly available hedge plant, which is used in fencing property perimeter in Kenerapallam, Palaghat Dt, Kerala. Foliage of the plant is thick and fruits are in abundance during the season. The inner core of the ripe fruit is delicious and of nutritive value and commonly consumed. After consumption, the seeds are discarded as they are nonedible. Since the *Annona squamosa* seed is available free of cost, only the carbonization of its involved for the waste water treatment. Therefore the main objective of this study was to evaluate the possibility of using dried *Annona squamosa* seed to develop a new low-cost activated carbon and study its application to remove methyl red from simulated wastewater. Granulized *Annona squamosa* seed was previously investigated to adsorb cationic dyes [18]. Systematic evaluation of the parameters involved, such as pH, adsorbent dose, adsorbent particle size, initial dye concentration and time.

### 2. Materials and Methods

#### 2.1. Preparation of activated carbon from the *Annona squamosa* seed (CAS)

The *Annona squamosa* seed was air-dried and powdered in a grinder. It was soaked in concentrated H<sub>2</sub>SO<sub>4</sub> for 12 hours and washed thoroughly with distilled water till it attained neutral pH and soaked in two percent NaHCO<sub>3</sub> overnight in order to remove any excess acid present. Then the material was washed with distilled water and dried at 110±2°C. The

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dry biomass was crushed into granules, sieved to different particle sizes, and then preserved in desiccators for use.

## 2.2. Preparation of synthetic solutions

A stock solution of 500 mg L<sup>-1</sup> was prepared by dissolving the appropriate amount of MR (obtained from s.d.Fine Chemicals, Mumbai, India) in 100 mL and made to 1000 mL with distilled water. Different concentrations ranged between 25 and 200 mg L<sup>-1</sup> of MR were prepared from the stock solution. All the chemicals used throughout this study were of analytical-grade reagents. Double-distilled water was used for preparing all of the solutions and reagents. The initial pH was adjusted with 0.1 M HCl or 0.1 M NaOH. All the adsorption experiments were carried out at room temperature (27±2°C).

## 2.3. Batch adsorption studies

### 2.3.1. Effect of pH on MR adsorption

The effect of pH on the equilibrium uptake of dyes was investigated by employing an initial concentration of MR (100mg/L) and 0.6 g/50 mL of CAS. The initial pH values were adjusted with 0.1 M HCl or NaOH to form a series of pH from 2 to 10. The suspensions were shaken at room temperature (27±2°C) using agitation speed (150 rpm), the minimum contact time required to reach the equilibrium (100 min) and the amount of MR adsorbed determined.

### 2.3.2. Effect of CAS dose on MR adsorption

The effect of adsorbent dose on the equilibrium uptake of MR (100 mg L<sup>-1</sup>) was investigated with CAS concentrations of 0.2, 0.4 and 0.6 g/ 50mL. The experiments were performed by shaking known MR concentration with the above different CAS concentrations to the equilibrium uptake (100 min) and the amount of MR adsorbed was determined.

### 2.3.3. Kinetics studies

Adsorption studies were conducted in 250-mL shaking flasks at a solution pH of 7.0. CAS (0.2g/50mL) was thoroughly mixed individually with 50mL of MR solution (100 mg/L) and the suspensions were shaken at room temperature. Samples of 1.0 mL were collected from the duplicate flasks at required time intervals viz.10, 20,30,40,50,60,70,80,90 and100 min and were centrifuged for 5 min. The clear solutions were analyzed for residual MR concentration in the solutions.

### 2.3.4. Adsorption isotherm

Batch adsorption experiments were carried out in a rotary shaker at 150 rpm using 250ml-shaking flasks at room temperature for 100 min. The CAS (0.2 and 0.6 g) was thoroughly mixed with 50 mL of MR solutions. The isotherm studies were performed by varying the initial MR concentrations from 25 to 200 mg/L at pH 7.0, which was adjusted using 0.1 M HCl or 0.1 M NaOH before addition of CAS and maintained throughout the experiment. After shaking the flasks for 100 min, the reaction mixture was analyzed for the residual MR concentration.

The concentration of MR in solution was measured by using direct UV-vis spectrophotometric method using a Systronic Spectrophotometer-104 at wavelength of 540 nm. All the experiments were duplicated and only the mean values are reported. The maximum deviation observed was less than ±4%.

Adsorption of MR from simulated wastewater was studied using 0.2g / 50 mL of CAS and MR concentrations 100 mg /L at initial pH 7.0. The amount of dye adsorbed at equilibrium onto carbon,  $q_e$  (mg/g), was calculated by the following mass balance relationship:

$$q_e = (C_0 - C_e)V/W \quad (1)$$

where  $C_0$  and  $C_e$  (mg/L) are the initial and equilibrium liquid-phase concentration of MR, respectively,  $V$  is the volume of the solution(L), and  $W$  is the weight of the CAS used(g).

## 3. Results and Discussion

### 3.1. Effect of system pH on MR Uptake

The pH of the system exerts profound influence on the adsorptive uptake of adsorbate molecules presumably due to its influence on the surface properties of the adsorbent and ionization/dissociation of the adsorbate molecule. Figure 1 shows the variations in the removal of dye from wastewater at different system pH. From the figure, it is evident that the maximum removal of MR color is observed at pH 4. Similar trend of pH effect was observed for the adsorption of MR on activated carbon prepared from sugarcane bagasse [19], and *cucumis sativa* [20], which may be attributed to the hydrophobic nature of the developed carbon which led to absorb hydrogen ions (H<sup>+</sup>) onto the surface of the carbon when immersed in water and made it positively charged. Low pH value (1.0 to 3.0) leads to an increase in H<sup>+</sup> ion concentration in the system and the surface of the activated carbon acquires positive charge by absorbing H<sup>+</sup> ions. On the other hand, increase of the pH value led to increase of the number of negatively charged sites. As the CAS surface is negatively charged at high pH, a significantly strong electrostatic attraction appears between the negatively charged carbon surface

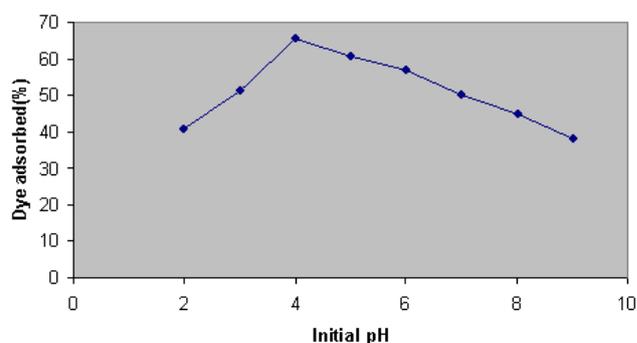


Figure 1: Effect of system pH on adsorption of MR (100 mg L<sup>-1</sup>) onto CAS (0.6 g /50mL) at room temperature (27±2 °C), agitation speed 150 rpm for the minimum contact time required to reach the equilibrium (100 min)

and cationic dye molecule leading to maximum adsorption of cationic dyes [21] from waste water. The lowest adsorption occurred at pH 2.0 and the highest adsorption occurred at pH~6.0. Adsorbents surface would be positively charged up to pH < 4, and heterogeneous in the pH range 4-6. Thereafter, it should be negatively charged. Moreover, the increasing in the adsorption of MR with decreasing of pH value is also due to the attraction between azo dye and excess H<sup>+</sup> ions in the solution.

### 3.2. Effect of contact time and initial MR concentration

The relation between removal of MR and reaction time were studied to see the rate of dye removal. The results of percentage removal of MR at pH 4.0 with increase of contact time using CAS are presented in Figure 2. It was found that more than 50% removal of MR concentration occurred in the first 50 min, and thereafter the rate of adsorption of the MR onto CAS were found to be slow. The rapid adsorption at the initial contact time is due to the highly negatively charged surface of the CAS for adsorption of MR in the solution at pH 4. Later slow rate of MR adsorption is probably due to the electrostatic hindrance or repulsion between the adsorbed negatively charged adsorbate species onto the surface of CAS and the available adsorbate species in the solution as well as the slow pore diffusion of the solute ions into the bulk of the adsorbent. The equilibrium was attained at 100 min when the maximum MR adsorption onto CAS was reached.

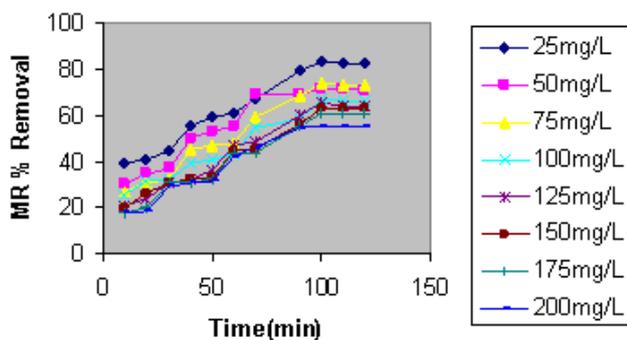


Figure 2: Effect of contact time on the removal of different initial concentrations of MR using CAS (0.2 g/50mL) at pH 4.0

Also, the effect of initial concentration of MR in the solution on the capacity of adsorption onto CAS was studied and is shown in Figure 2. The experiments were carried out at fixed adsorbent dose (0.2 g/50 mL) in the test solution at room temperature (27±2°C), pH 4 and at different initial concentrations of MR (25, 50, 75, 100, 125, 150, 175 and 200 mg L<sup>-1</sup>) for different time intervals (10, 20, 30, 40, 50, 60, 70, 80, 90 and 100 min). Figure 2 shows that the percentage of adsorption efficiency of CAS decreased with the increase of initial MR concentration in the solution. Though the percent adsorption decreased with increase in initial dye concentration, the actual amount of MR adsorbed per unit mass of adsorbent increased with increase in MR concentration in the test solution.

It is evident from Figure 2 that the amount adsorbed on the solid phase CAS at a lower initial concentration of MR was smaller than the corresponding amount when higher initial concentrations were used. However, the percentage removal of MR was greater at lower initial concentrations and smaller at higher initial concentrations. The adsorption capacity for CAS was increased from 5.176 to 27.68 mg g<sup>-1</sup> as the MR concentration increased from 25 to 200 mg L<sup>-1</sup>. In the process of MR adsorption initially dye molecules have to first encounter the boundary layer effect and then it has to diffuse from boundary layer film onto adsorbent surface and then finally, it has to diffuse into the porous structure of the adsorbent. This phenomenon will take relatively longer contact time.

### 3.3. Effect of adsorbent mass on MR adsorption

The adsorption of MR on CAS was studied by changing the quantity of adsorbent (0.2, 0.3, 0.4, 0.5 and 0.6 g/50 mL) in the test solution while keeping the initial MR concentration (100 mg L<sup>-1</sup>), temperature (27±2°C) and pH (4.0) constant at contact times for 100 min (Figure 3). The adsorption increased from 66.67% to 75.86%, as the CAS dose increased from 0.2 g to 0.6 g/50 mL at equilibrium time (100 min). Maximum MR removal was achieved within 10-50 min after which MR concentration in the reaction solution was almost constant. Increase in the adsorption with adsorbent dose can be attributed to increased MR surface area and availability of more adsorption sites, while the unit adsorbed of MR decreased with increase in CAS dose.

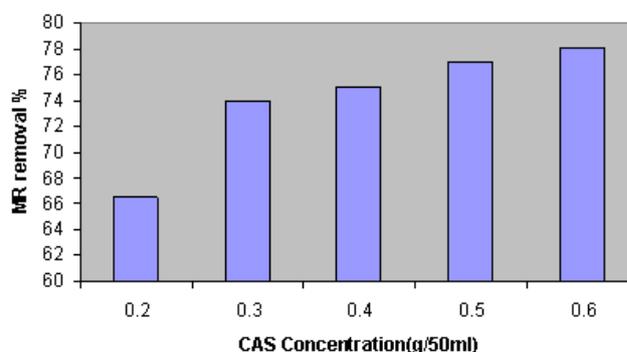


Figure 3: Effect of adsorbent concentration on MR removals (C0: 100 mg L<sup>-1</sup>, pH 4.0, agitation speed: 150 rpm, temperature: 27±2°C)

### 3.4. Isotherm data analysis

The relationship between the amount of a substance adsorbed at constant temperature and its concentration in the equilibrium solution is called the adsorption isotherm. The adsorption isotherm is important from both a theoretical and a practical point of view. In order to optimize the design of an adsorption system to remove the dye, it is important to establish the most appropriate correlations of the equilibrium data of each system. Equilibrium isotherm equations are used to describe the experimental adsorption data. The parameters

obtained from the different models provide important information on the adsorption mechanisms and the surface properties and affinities of the adsorbent. The most widely accepted surface adsorption models for single-solute systems are the Langmuir and Freundlich models. The correlation with the amount of adsorption and the liquid-phase concentration was tested with the Langmuir, Freundlich, Tempkin and Dubinin-Radushkevich (D-R) isotherm equations. Linear regression is frequently used to determine the best-fitting isotherm, and the applicability of isotherm equations is compared by judging the correlation coefficients.

### 3.4.1. Langmuir isotherm

The theoretical Langmuir isotherm [22] is valid for adsorption of a solute from a liquid solution as monolayer adsorption on a surface containing a finite number of identical sites. Langmuir isotherm model assumes uniform energies of adsorption onto the surface without transmigration of adsorbate in the plane of the surface [23]. Therefore, the Langmuir isotherm model was chosen for estimation of the maximum adsorption capacity corresponding to complete monolayer coverage on the adsorbent surface. The Langmuir non-linear equation is commonly expressed as followed:

$$q_e = \frac{Q_m K_a C_e}{1 + K_a C_e} \quad (2)$$

where,  $Q_m$  is a constant and reflect a complete monolayer ( $\text{mg g}^{-1}$ );  $K_a$  is adsorption equilibrium constant ( $\text{L mg}^{-1}$ ) that is related to the apparent energy of sorption. The Langmuir isotherm Equation 2 can be linearized [24, 25], as shown in Equation 3.

$$\frac{C_e}{q_e} = \frac{1}{K_a Q_m} + \frac{1}{Q_m} \times C_e \quad (3)$$

A plot of  $C_e/q_e$  versus  $C_e$  should indicate a straight line of slope  $1/Q_m$  and an intercept of  $1/(K_a Q_m)$ . The results obtained from the Langmuir model for the removal of MR onto CAS are shown in Table 1. The correlation coefficients reported in Table 1 showed strong positive evidence on the adsorption of MR onto CAS follows the Langmuir isotherm. The applicability of the linear form of Langmuir model to CAS was proved by the high correlation coefficients  $R^2 > 0.95$ . This suggests that the Langmuir isotherm provides a good model of the sorption system. The maximum monolayer capacity  $Q_m$  obtained from the Langmuir is 40.486  $\text{mg g}^{-1}$ .

### 3.4.2. The Freundlich isotherm

The Freundlich isotherm model [25] is the earliest known equation describing the adsorption process. It is an empirical equation and can be used for non-ideal sorption that involves heterogeneous adsorption. The Freundlich isotherm can be derived assuming a logarithmic decrease in the enthalpy of adsorption with the increase in the fraction of occupied sites and is commonly given by the following non-linear equation:

$$q_e = K_F C_e^{1/n} \quad (4)$$

Table 1: Comparison of the coefficients isotherm parameters for MR adsorption onto CAS (CAS concentration: 0.2 g/50 ml)

<b>Langmuir:</b>	
$Q_m$ ( $\text{mg g}^{-1}$ )	40.486
$K_a$ ( $\text{L}^{-1}$ )	0.0248
$R^2$	0.9491
<b>Freundlich:</b>	
$1/n$	0.5931
$K_F$ ( $\text{mg}^{-1}$ )	2.0583
$R^2$	0.9396
<b>Tempkin:</b>	
$\alpha$ ( $\text{L}^{-1}$ )	0.2032
$\beta$ ( $\text{mg}^{-1}$ )	8.0501
$b$	309.83
$R^2$	0.9386
<b>Dubinin-Radushkevich:</b>	
$Q_m$ ( $\text{mg}^{-1}$ )	25.134
$K$ ( $\times 10^{-5} \text{mol}^2 \text{kJ}^{-2}$ )	0.04
$E$ ( $\text{kJmol}^{-1}$ )	0.118
$R^2$	0.9203

where  $K_F$  is a constant for the system, related to the bonding energy.  $K_F$  can be defined as the adsorption or distribution coefficient and represents the quantity of dye adsorbed onto adsorbent for unit equilibrium concentration.  $1/n$  is indicating the adsorption intensity of dye onto the adsorbent or surface heterogeneity, becoming more heterogeneous as its value gets closer to zero. A value for  $1/n$  below 1 indicates a normal Langmuir isotherm while  $1/n$  above 1 is indicative of cooperative adsorption. Equation 4 can be linearized in the logarithmic form (Equation 5) and the Freundlich constants can be determined:

$$\log q_e = \log K_F + \frac{1}{n} \log C_e \quad (5)$$

The applicability of the Freundlich adsorption isotherm was also analyzed, using the same set of experimental data, by plotting  $\log q_e$  versus  $\log C_e$ . The data obtained from linear Freundlich isotherm plot for the adsorption of the MR onto CAS is presented in Table 1. The correlation coefficients ( $> 0.94$ ) showed that the Freundlich model is comparable to the Langmuir model. The  $1/n$  is lower than 1.0, indicating that MR is favorably adsorbed by CAS.

### 3.4.3. The Tempkin isotherm

Tempkin adsorption isotherm model was used to evaluate the adsorption potentials of the CAS for MR. The derivation of the Tempkin isotherm assumes that the fall in the heat of adsorption is linear rather than logarithmic, as implied in the Freundlich equation. The Tempkin isotherm has commonly been applied in the following form [26–28]:

$$q_e = \frac{RT}{b} \ln(AC_e) \quad (6)$$

The Tempkin isotherm, Equation 6, can be simplified to the following equation:

$$q_e = \beta \ln \alpha + \beta \ln C_e \quad (7)$$

where  $\beta = (RT)/b$ ,  $T$  is the absolute temperature in Kelvin and  $R$  is the universal gas constant,  $8.314 \text{ J (mol K)}^{-1}$ . The constant  $b$  is related to the heat of adsorption [29, 30]. The adsorption data were analyzed according to the linear form

of the Tempkin isotherm Equation 7. Examination of the data shows that the Tempkin isotherm fitted well the MR adsorption data for CAS. The linear isotherm constants and coefficients of determination are presented in Table 1. The correlation coefficients  $R^2$  obtained from Tempkin model were comparable to that obtained for Langmuir and Freundlich equations, which explain the applicability of Tempkin model to the adsorption of MR onto CAS.

#### 3.4.4. The Dubinin-Radushkevich (D-R) isotherm

The D-R model was also applied to estimate the porosity apparent free energy and the characteristics of adsorption [31–33]. The D-R isotherm does not assume a homogeneous surface or constant adsorption potential. The D-R model has commonly been applied in the following Equation 8 and its linear form, Equation 9.

$$q_e = Q_m \exp(-K\varepsilon^2) \quad (8)$$

$$\ln q_e = \ln Q_m - K\varepsilon^2 \quad (9)$$

where  $K$  is a constant related to the adsorption energy,  $Q_m$  is the theoretical saturation capacity,  $\varepsilon$  is the Polanyi potential, calculated from Eq. (10).

$$\varepsilon = RT \ln \left( 1 + \frac{1}{C_e} \right) \quad (10)$$

The slope of the plot of  $\ln q_e$  versus  $\varepsilon^2$  gives  $K$  ( $\text{mol}^2 \text{kJ}^{-2}$ ) and the intercept yields the adsorption capacity,  $Q_m$  ( $\text{mg g}^{-1}$ ). The mean free energy of adsorption ( $E$ ), defined as the free energy change when one mole of ion is transferred from infinity in solution to the surface of the solid, was calculated from the  $K$  value using Equation 11[34]:

$$E = \frac{1}{\sqrt{2K}} \quad (11)$$

The calculated value of D-R parameters is given in Table 1. The saturation adsorption capacity  $Q_m$  obtained using D-R isotherm model for adsorption of MR onto CAS is  $25.134 \text{ mg g}^{-1}$  at  $0.2 \text{ g}/50 \text{ mL}$  adsorbent dose, which is close to that obtained ( $18.38 \text{ mg g}^{-1}$ ) from second order kinetic model (Table 2). The values of  $E$  calculated using Equation 11 is  $0.118 \text{ kJ mol}^{-1}$ , which indicating that the physico-adsorption process plays the significant role in the adsorption of MR onto CAS.

Table 2: Comparison of the first- and second-order adsorption rate constants and calculated and experimental  $q_e$  values: initial MR  $100 \text{ mg L}^{-1}$  and CAS  $0.2 \text{ g}/50 \text{ mL}$

Experimental	First-order kinetic model			Second-order kinetic model			
	$q_e$	$k_1$	$q_e$	$R^2$	$k_2$	$q_e$	$h$
18.713	0.0009	57.17	0.982	0.006	18.38	1.92	0.991

#### 3.5. Kinetic models applied to the adsorption of MR onto CAS

Several steps can be used to examine the controlling mechanism of adsorption process such as chemical reaction, diffusion control and mass transfer; kinetic models are used to

test experimental data from the adsorption of MR onto CAS. The kinetics of MR adsorption onto CAS is required for selecting optimum operating conditions for the full-scale batch process. The kinetic parameters, which are helpful for the prediction of adsorption rate, give important information for designing and modeling the adsorption processes. Thus, the kinetics of MR adsorption onto CAS were analyzed using pseudo-first-order [35], pseudo-second-order [36], Elovich [37–39] and intraparticle diffusion [40, 41] kinetic models. The conformity between experimental data and the model-predicted values was expressed by the correlation coefficients ( $R^2$ , values close or equal to 1). The relatively higher value is the more applicable model to the kinetics of MR adsorption onto CAS.

##### 3.5.1. Pseudo-first-order equation

The adsorption kinetic data were described by the Lagergren pseudo-first-order model [35], which is the earliest known equation describing the adsorption rate based on the adsorption capacity. The differential equation is generally expresses as follows:

$$\frac{dq_t}{dt} = k_1(q_e - q_t) \quad (12)$$

where  $q_e$  and  $q_t$  are the adsorption capacity at equilibrium and at time  $t$ , respectively ( $\text{mg g}^{-1}$ ),  $k_1$  is the rate constant of pseudo-first-order adsorption ( $\text{L min}^{-1}$ ). Integrating Equation 12 for the boundary conditions  $t = 0$  to  $t$  and  $q_t = 0$  to  $q_t$  gives:

$$\log \left( \frac{q_e}{q_e - q_t} \right) = \frac{k_1}{2.303} t \quad (13)$$

Equation 13 can be rearranged to obtain the following linear form:

$$\log(q_e - q_t) = \log(q_e) - \frac{k_1}{2.303} t \quad (14)$$

In order to obtain the rate constants, the values of  $\log(q_e - q_t)$  were linearly correlated with  $t$  from which  $k_1$  and predicted  $q_e$  can be determined from the slope and intercept of the plot, respectively (Figure 4). The variation in rate should be proportional to the first power of concentration for strict

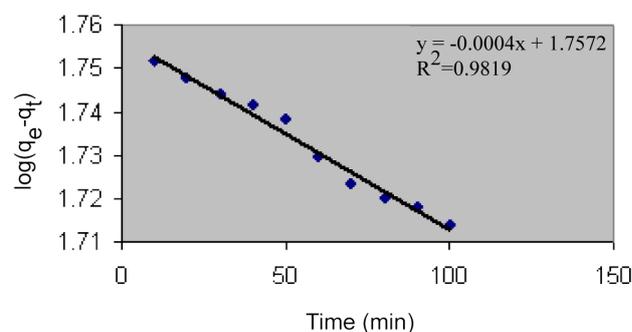


Figure 4: Pseudo-first-order kinetics for MR ( $100 \text{ mg L}^{-1}$ ) adsorption onto CAS. Conditions: adsorbent dosage  $0.2 \text{ g}/50 \text{ mL}$ , pH 4.0, temperature  $27 \pm 2^\circ \text{C}$

surface adsorption. However, the relationship between initial solute concentration and rate of adsorption will not be linear when pore diffusion limits the adsorption process. Figure 4 shows that the pseudo-first-order equation fits well for the first 50 min and thereafter the data deviate from theory. Thus, the model represents the initial stages where rapid adsorption occurs well but cannot be applied for the entire adsorption process. Furthermore, the correlation coefficient  $R^2$  are relatively low for most adsorption data and the adsorption maximum obtained was differ from the experimental value (Table 2). This shows that the adsorption of MR onto CAS cannot be applied and the reaction mechanism is not a first-order reaction.

### 3.5.2. Pseudo-second-order equation

The adsorption kinetic may be described by the pseudo-second-order model [36]. The differential equation is generally given as follows:

$$\frac{dq_t}{dt} = k_2(q_e - q_t)^2 \quad (15)$$

where  $k_2$  ( $\text{g} (\text{mg min})^{-1}$ ) is the second-order rate constant of adsorption. Integrating Equation 15 for the boundary conditions  $q_t = 0$  to  $q_t$  at  $t = 0$  to  $t$  and rearranging gives the following linear form:

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \quad (16)$$

The second-order rate constants were used to calculate the initial sorption rate, given by the following equation:

$$h = k_2 q_e^2 \quad (17)$$

If the second-order kinetics is applicable, then the plot of  $t/q_t$  versus  $t$  should show a linear relationship. Values of  $k_2$  and equilibrium adsorption capacity  $q_e$  were calculated from the intercept and slope of the plot of  $t/q_t$  versus  $t$  (Figure 5). The linear plots of  $t/q_t$  versus  $t$  show good agreement between experimental and calculated  $q_e$  values at 100mg/L initial MR and 0.2 mg/50 mL adsorbent concentrations (Table 2). The correlation coefficients for the second-order kinetic model are greater than 0.99 and the adsorption maximum obtained was close to the experimental value, which led to believe that the pseudo-second-order kinetic model provided good correlation for the bioadsorption of MR onto CAS. The values of initial sorption ( $h$ ) that represents the rate of initial adsorption, is  $1.920 \text{ mg} (\text{g min})^{-1}$  with 100 mg/L MR concentrations onto CAS dose  $0.2 \text{ g mL}^{-1}$  (Table 2).

### 3.5.3. Elovich equation

The Elovich equation is another rate equation based on the adsorption capacity generally expressed as following [37–39]:

$$\frac{dq_t}{dt} = B_E \exp(-A_E q_t) \quad (18)$$

where  $B_E$  is the initial adsorption rate ( $\text{mg} (\text{g min})^{-1}$ ) and  $A_E$  is the de-sorption constant ( $\text{g mg}^{-1}$ ) during any experiment.

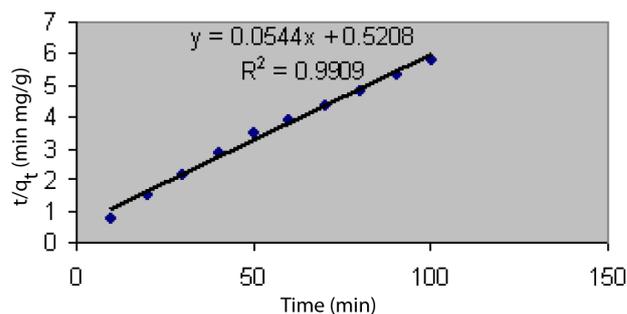


Figure 5: Pseudo-second-order kinetics for MR ( $100 \text{ mg L}^{-1}$ ) adsorption onto CAS. Conditions: adsorbent dosage  $0.2 \text{ g/50 mL}$ , pH 4.0, temperature  $27 \pm 2^\circ \text{C}$

Equation 18 can be simplified by assuming  $A_E B_E t \gg t$  and by applying the boundary conditions  $q_t = 0$  at  $t = 0$  and  $q_t = q_t$  at  $t$ :

$$q_t = \frac{1}{A_E} \ln(B_E A_E) + \frac{1}{A_E} \ln(t) \quad (19)$$

If MR adsorption by CAS fits the Elovich model, a plot of  $q_t$  versus  $\ln(t)$  should yield a linear relationship with a slope of  $1/A_E$  and an intercept of  $1/A_E \ln(A_E B_E)$  (Figure 6). Thus, the constants can be obtained from the slope and the intercept of the straight line (Table 3). The initial adsorption rate  $B_E$  was  $33.26 \text{ mg} (\text{g min})^{-1}$  for initial MR concentration  $100 \text{ mg L}^{-1}$  on CAS dose of  $0.2 \text{ g mL}^{-1}$ . The desorption constant,  $A_E$  was  $0.4346 \text{ g mg}^{-1}$  for initial MR concentration  $100 \text{ mg L}^{-1}$  over CAS dose of  $0.2 \text{ g mL}^{-1}$  (Table 3).

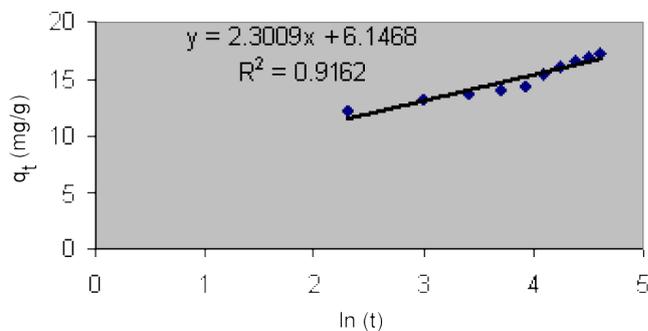


Figure 6: Elovich model plot for MR ( $100 \text{ mg L}^{-1}$ ) adsorption onto CAS. Conditions: adsorbent dosage  $0.2 \text{ g/50 mL}$ , pH 4.0, temperature  $27 \pm 2^\circ \text{C}$

Table 3: Parameters obtained from Elovich kinetics model and intraparticle diffusion model using initial MR concentration  $100 \text{ mg L}^{-1}$

Elovich			Intraparticle diffusion		
$A_E$	$B_E$	$R^2$	$K_{\text{dif}}$	$C$	$R^2$
0.43	33.26	0.917	0.78	9.408	0.974

### 3.5.4. The intraparticle diffusion model

The adsorbate species are most probably transported from the bulk of the solution into the solid phase through intraparticle diffusion/transport process, which is often the rate-limiting step in many adsorption processes, especially in a

rapidly stirred batch reactor [42]. Since the MR are probably transported from its aqueous solution to the CAS by intraparticle diffusion, so the intraparticle diffusion is another kinetic model should be used to study the rate of MR adsorption onto CAS. The possibility of intraparticle diffusion was explored by using the intraparticle diffusion model, which is commonly expressed by the following equation:

$$q_t = K_{\text{dif}} t^{1/2} + C \quad (20)$$

where  $C$  ( $\text{mg g}^{-1}$ ) is the intercept and  $K_{\text{dif}}$  is the intraparticle diffusion rate constant (in  $\text{mg g}^{-1} \text{min}^{-1/2}$ ). The values of  $q_t$  were found to be linearly correlated with values of  $t^{1/2}$  (Figure 7) and the rate constant  $K_{\text{dif}}$  directly evaluated from the slope of the regression line (Table 3). The value of intercept  $C$  (Table 3) provide information about the thickness of the boundary layer, the resistance to the external mass transfer increase as the intercept increase. The constant  $C$  was found to be 9.4084 for the dye concentration  $100 \text{ mg L}^{-1}$ , which indicating the increase of the thickness of the boundary layer and decrease of the chance of the external mass transfer and hence increase of the chance of internal mass transfer. The  $R^2$  values given in Table 3 are close to unity indicating the application of this model. This may confirm that the rate-limiting step is the intraparticle diffusion process. The intraparticle diffusion rate constant,  $K_{\text{dif}}$ , was  $0.7758 \text{ g}^{-1} \text{min}^{-1/2}$ . The linearity of the plots demonstrated that intraparticle diffusion played a significant role in the uptake of the adsorbate by adsorbent. However, As still there is no sufficient indication about it, Ho [43] has shown that if the intraparticle diffusion is the sole rate-limiting step, it is essential for the  $q_t$  versus  $t^{1/2}$  plots to pass through the origin, which is not the case in Figure 7, it may be concluded that surface adsorption and intraparticle diffusion were concurrently operating during the MR and CAS interactions.

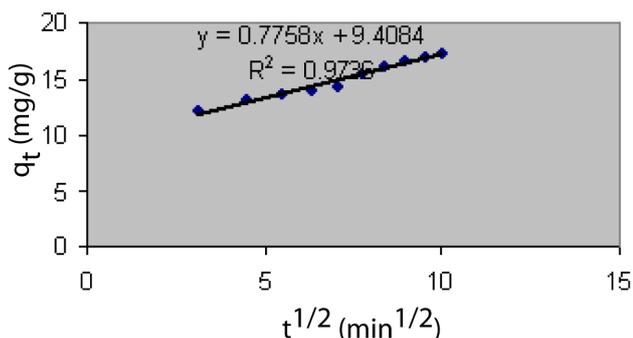


Figure 7: Intraparticle diffusion plot for MR ( $100 \text{ mg L}^{-1}$ ) adsorption onto CAS. Conditions: adsorbent dosage  $0.2 \text{ g/50 mL}$ , pH 4.0, temperature  $27 \pm 2^\circ \text{C}$

#### 4. Conclusion

The results of this investigation show that activated carbon developed from *Annona squamosa* seed has a suitable adsorption capacity for the removal of MR from aqueous solutions. The equilibrium adsorption is practically

achieved in 100 min. The experimental results were analyzed by using Langmuir, Freundlich, Tempkin and Dubinin-Radushkevich isotherm models and the correlation coefficients for Langmuir, Freundlich, Tempkin and Dubinin-Radushkevich equations are well fitted. Adsorption behavior is described by a monolayer Langmuir-type isotherm. The kinetic study of MR on CAS was performed based on pseudo-first-order, pseudo-second-order, Elovich and intraparticle diffusion equations. The data indicate that the adsorption kinetics follow the pseudo-second-order rate with intraparticle diffusion as one of the rate determining steps. The present study concludes that the CAS could be employed as low-cost adsorbents as alternatives to commercial activated carbon for the removal of color and dyes from water and wastewater.

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