# EFFECTS OF THERMAL CONDUCTIVITY OF FLUID ON FREE CONVECTION FLOW ALONG A VERTICAL FLAT PLATE WITH TRANSVERSE CONDUCTION

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**Abstract:** This paper reports the effects of transverse conduction variation with thermal conductivity on free convection flow along a vertical flat plate. The governing equations with associated boundary conditions reduce to local non-similarity boundary layer equations for this phenomenon are converted to dimensionless forms using a suitable transformation. The transformed non-linear equations are then solved using the implicit finite difference method together with Keller-box technique. Numerical results of the velocity and temperature profiles, skin friction and surface temperature profiles for different values of the thermal conductivity parameter, the Prandtl number and the transverse conduction variation parameters are presented graphically. Detailed discussion is given for the effect of the aforementioned parameters. Mentionable effect is found in skin friction and surface temperature for the transverse conduction variation parameter.

Keywords: thermal conductivity, transverse conduction variation, Grashof number, Prandtl number.

#### NOMENCLATURE

- $C_{fx}$  Local skin friction coefficient
- $C_p$  Specific heat at constant pressure
- *f* Dimensionless stream function
- *g* Acceleration due to gravity
- *h* Dimensionless temperature
- *T* Temperature of the interface
- $T_b$  Temperature at outside surface of the plate
- $T_f$  Temperature of the fluid
- $T_{\underline{\infty}}$  Temperature of the ambient fluid
- $\overline{u}$  Velocity component in *x* direction
- $\overline{v}$  Velocity component in *y*-direction
- *u* Dimensionless velocity component in *x* direction
- $\frac{v}{2}$  Dimensionless velocity component in y- direction
- $\overline{x}$  Cartesian co-ordinates
- $\overline{\mathcal{Y}}$  Cartesian co-ordinates

- *x* Dimensionless Cartesian co-ordinates
- *y* Dimensionless Cartesian co-ordinates

# **GREEK SYMBOLS**

- $\gamma$  Thermal conductivity of the fluid
- $\lambda$  Transverse conduction variation of plate
- $\nabla$  Vector differential operator
- $\eta$  Similarity variable
- $\kappa_{\infty}$  Thermal conductivity of the ambient fluid
- $K_s$  Thermal conductivity of the solid
- $\kappa_f$  Thermal conductivity of the fluid
- <sup>J</sup> Viscosity of the fluid
- $\mu$  Kinematic viscosity
- Density of the fluid inside the boundary layer
- $\rho$  Shearing stress
- $\tau_w$  Stream function

# **INTRODUCTION**

Effects of thermal conductivity of fluid and transverse conduction variation problems on free convection flow are important from the technical point of view and such types of problems have received much attention by many researchers in electronics and in physics broadly.

Miyamoto et al.<sup>1</sup> studied the effect of axial heat conduction in a vertical flat plate on free convection heat transfer. Pozzi and Lupo<sup>2</sup> investigated the coupling of conduction with laminar convection along a flat plate. Khan<sup>3</sup> analyzed the conjugate effect of conduction and convection with natural convection flow from a vertical flat plate and in an inclined square cavity. Mamun<sup>4</sup> studied the effects of conduction and convection on magnetohydrodynamic flow with and without viscous dissipation from a vertical flat plate. Rahman et al.<sup>5</sup> investigated the effects of temperature dependent thermal conductivity on MHD free convection flow along a vertical flat plate with heat conduction. Nasrin and Alim<sup>6</sup> studied the combined effects of viscous dissipation and temperature dependent thermal conductivity on MHD free convection flow with conduction and joule heating along a vertical flat plate. Alim et al.<sup>7</sup> analyzed the combined effect of viscous dissipation & joule heating on the coupling of conduction & free convection along a vertical flat plate. Alim et al.<sup>8</sup> investigated Joule heating effect on the coupling of conduction with MHD free convection flow from a vertical flat plate. Chowdhury and Islam<sup>13</sup> analyzed MHD Free Convection Flow of Visco-elastic Fluid past an Infinite Porous Plate. Alam et al.<sup>14</sup> studied viscous dissipation effects on MHD natural convection flow over a sphere in the presence of heat generation.

The present study is to incorporate the idea of the effects of thermal conductivity of fluid on natural convective boundary layer flow along a vertical flat plate with transverse conduction variation.

#### MATHEMATICAL FORMULATION

At first we consider a steady two-dimensional laminar natural convection flow of a viscous and incompressible fluid along a vertical insulated top and bottom tip flat plate of length l and thickness b (Figure-1). It is assumed that the temperature at the outer surface of the plate is maintained at a constant temperature  $T_b$ , where  $T_b > T_\infty$  the ambient temperature of the fluid. In this work  $\overline{y}$  -axis i.e. normal direction to the surface and  $\overline{x}$  -axis is taken along the flat plate. The coordinate system and the configuration are shown in Fig. 1.

The governing equations of such laminar flow with thermal conductivity and also transverse conduction variation along a vertical flat plate under the Boussinesq approximations  $\rho = \rho_{\infty}[1 - \beta(T_b - T_{\infty})]$ , where  $\rho_{\infty}$  and  $T_{\infty}$  are the density and temperature respectively outside the boundary layer. For the present problem for continuity, momentum and energy equations take the following forms



Figure 1. Physical model and coordinate system.

$$\frac{\partial \overline{u}}{\partial \overline{x}} + \frac{\partial \overline{v}}{\partial \overline{y}} = 0 \tag{1}$$

$$\overline{u}\frac{\partial\overline{u}}{\partial\overline{x}} + \overline{v}\frac{\partial\overline{u}}{\partial\overline{y}} = v\frac{\partial^2\overline{u}}{\partial\overline{y}^2} + g\beta(T_f - T_\infty)$$
(2)

$$\overline{u}\frac{\partial T_f}{\partial \overline{x}} + \overline{v}\frac{\partial T_f}{\partial \overline{y}} = \frac{1}{\rho}\frac{\partial}{C_p}\left(\kappa_f\frac{\partial T_f}{\partial \overline{y}}\right)$$
(3)

Here  $\beta$  is coefficient of volume expansion. The temperature dependent thermal conductivity, which is used by Rahman<sup>5</sup> as follows

$$\kappa_f = \kappa_\infty [1 + \delta (T_f - T_\infty)] \tag{4}$$

Where  $\kappa_{\infty}$  is the thermal conductivity of the ambient fluid and  $\delta$  is a constant, defined as

$$\delta = \frac{1}{\kappa_f} \left( \frac{\partial \kappa}{\partial T} \right)_f$$

The appropriate boundary condition to be satisfied by the above equations are

$$\overline{u} = 0, \ \overline{v} = 0$$

$$T_f = T(\overline{x}, 0), \ \frac{\partial T_f}{\partial \overline{y}} = \frac{\kappa_s}{b\kappa_f} (T_f - T_b)$$

$$on \ \overline{y} = 0, \ \overline{x} > 0$$

$$\overline{u} \to 0, \ T_f \to T_{\infty} \text{ as } \ \overline{y} \to \infty, \ \overline{x} > 0$$

$$(5)$$

The non-dimensional governing equations and boundary conditions can be obtained from equations (1) - (3) using the following dimensionless quantities

$$x = \frac{\overline{x}}{l}, \quad y = \frac{\overline{y}}{l}Gr^{\frac{1}{4}}, \quad u = \frac{\overline{u}l}{\upsilon}Gr^{-\frac{1}{2}}, \quad v = \frac{\overline{v}l}{\upsilon}Gr^{-\frac{1}{4}}, \quad (6)$$
$$\theta = \frac{T_f - T_{\infty}}{T_b - T_{\infty}}, \quad Gr = \frac{g\beta l^3(T_b - T_{\infty})}{\upsilon^2}$$

where l is the length of the plate, Gr is the Grashof number,  $\theta$  is the dimensionless temperature.

Now from equations (1)-(3), we get using the following dimensionless equations

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{7}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} = \frac{\partial^2 u}{\partial y^2} + \theta$$
(8)

$$u\frac{\partial\theta}{\partial x} + v\frac{\partial\theta}{\partial y} = \frac{1}{\Pr}(1 + \gamma\theta)\frac{\partial^2\theta}{\partial y^2} + \frac{\gamma}{\Pr}\left(\frac{\partial\theta}{\partial y}\right)^2 \quad (9)$$

where  $\Pr = \frac{\mu C_p}{\kappa_{\infty}}$  is the Prandtl number,  $\gamma = \delta(T_b - T_{\infty})$  is the non-dimensional thermal conductivity variation parameter for fluid. The

Journal of Mechanical Engineering, Vol. ME 44, No. 2, December 2014 Transaction of the Mechanical Engineering Division, The Institution of Engineers, Bangladesh corresponding boundary conditions (5) then take the following form

$$u = 0, v = 0, \theta - 1 = (1 + \gamma \theta) \lambda \frac{\partial \theta}{\partial y} \text{ on } y = 0, x > 0$$
(10)  
$$u \to 0, \theta \to 0 \text{ as } y \to \infty, x > 0$$

here  $\lambda = \left(\frac{\kappa_{\infty}b}{\kappa_s l}\right) Gr^{\frac{1}{4}}$  is the transverse conduction

variation parameter. The described problem is governed by this parameter  $\lambda$ .

To solve the equations (8) and (9) subject to the boundary conditions (10) the following transformations are proposed by Merkin &  $Pop^9$ 

$$\psi = x^{\frac{4}{5}} (1+x)^{-\frac{1}{20}} f(x,\eta)$$
  

$$\eta = y x^{-\frac{1}{5}} (1+x)^{-\frac{1}{20}}$$
  

$$\theta = x^{\frac{1}{5}} (1+x)^{-\frac{1}{5}} h(x,\eta)$$
(11)

here  $\eta$  is the similarity variable and  $\psi$  is the non-dimensional stream function which satisfies the continuity equation and is related to the velocity components in the usual way as

$$u = \frac{\partial \psi}{\partial y}$$
 and  $v = -\frac{\partial \psi}{\partial x}$ 

Moreover,  $h(x, \eta)$  represents the non-dimensional temperature. The momentum and energy equations are transformed for the new co-ordinate system. At first, the velocity components are expressed in terms of the new variables for this transformation. Thus the following equations

$$f''' + \frac{16+15x}{20(1+x)} ff''' - \frac{6+5x}{10(1+x)} f'^{2} + h = x \left( f' \frac{\partial f'}{\partial x} - f'' \frac{\partial f}{\partial x} \right)$$
(12)

$$\frac{1}{\Pr} h'' + \frac{\gamma}{\Pr} \left(\frac{x}{1+x}\right)^{\frac{1}{5}} hh'' + \frac{\gamma}{\Pr} \left(\frac{x}{1+x}\right)^{\frac{1}{5}} h'^2 + \frac{16+15x}{20(1+x)} fh'$$

$$-\frac{1}{5(1+x)} fh = x \left(f' \frac{\partial h}{\partial x} - h' \frac{\partial f}{\partial x}\right)$$
(13)

where prime denotes partial differentiation with respect to  $\eta$ . The boundary conditions as mentioned in equation (10) then take the following form

$$f(x,0) = f'(x,0) = 0$$

$$h'(x,0) = \frac{x^{\frac{1}{5}}(1+x)^{-\frac{1}{5}}h(x,0) - 1}{\lambda(1+x)^{-\frac{1}{4}} + \gamma x^{\frac{1}{5}}(1+x)^{-\frac{9}{20}}h(x,0)}$$

$$f'(x,\infty) \to 0, \quad h(x,\infty) \to 0$$
(14)

From the process of numerical computation, in practical point of view, it is important to calculate the

values of the surface shear stress in terms of the skin friction coefficient. This can be written in the non-dimensional form as Molla et al.<sup>10</sup>

$$C_f = \frac{Gr^{-\frac{3}{4}}l^2}{\mu\nu}\tau_w \tag{15}$$

where  $\tau_w [= \mu (\partial \ \overline{u} / \partial \ \overline{y})_{\overline{y} = 0}]$  is the shearing stress. Using the new variables described in (6), the local skin friction can be written as

$$C_{fx} = x^{\frac{2}{5}} (1+x)^{-\frac{3}{20}} f''(x,0)$$
(16)

In practical point of view, it is important to calculate the values of the surface temperature. The numerical values of the surface temperature are obtained from the relation. This can written in the non-dimensional form as

$$\theta(x,0) = x^{\frac{1}{5}}(1+x)^{-\frac{1}{5}}h(x,0)$$
(17)

### ACCURACY TEST OF THE RESULT

Table 1 and Table 2 depict the comparisons of the present numerical results of the skin friction  $C_{fx}$  and the surface temperature  $\theta(x,0)$  with those obtained by Pozzi & Lopo<sup>2</sup> and Merkin & Pop<sup>9</sup> respectively. Here, the thermal conductivity and transverse conduction variation parameters are ignored (i.e.  $\gamma = 0$  &  $\lambda = 0$ ) and the Prandtl number Pr = 0.733 with  $x^{\frac{1}{5}} = \xi$  is chosen. It is clearly seen that there is an excellent agreement among the present results with the solutions Pozzi & Lopo<sup>2</sup> and Merkin & Pop<sup>9</sup>.

Table 1. Comparison of the skin friction  $C_{fx}$  with Prandtl number Pr = 0.733,  $\gamma = 0$  and  $\lambda = 0$ .

$C_{fx}$				
1	Pozzi &	Merkin &	Present	
$x^{\overline{5}} = \xi$	Lupo <sup>2</sup>	Pop <sup>9</sup>	work	
0.1	0.014	0.014	0.015	
0.4	0.172	0.172	0.170	
0.5	0.250	0.250	0.272	
0.6	0.337	0.337	0.340	
0.7	0.430	0.430	0.423	
0.8	0.530	0.530	0.528	
0.9	0.635	0.635	0.633	
1.0	0.741	0.745	0.748	
1.2	0.817	0.972	0.972	

#### NUMERICAL METHOD OF SOLUTION

This paper investigates the effects of thermal conductivity of fluid on natural convective boundary layer flow along a vertical flat plate with transverse conduction variation. The set of equations (12) and (13) together with the boundary conditions (14) are solved by applying implicit finite difference method with Keller-box elimination technique<sup>11</sup>, which is well documented by Cebeci and Bradshaw<sup>12</sup>.

$\theta(x,0)$				
1	Pozzi &	Merkin &	Present	
$x^5 = \xi$	Lupo <sup>2</sup>	Pop <sup>9</sup>	work	
0.1	0.177	0.177	0.204	
0.4	0.493	0.493	0.481	
0.5	0.557	0.557	0.580	
0.6	0.608	0.608	0.615	
0.7	0.651	0.651	0.651	
0.8	0.684	0.686	0.687	
0.9	0.708	0.715	0.716	
1.0	0.717	0.741	0.742	
1.2	0.640	0.781	0.781	

Table 2. Comparison of the surface temperature  $\theta(x,0)$  with Prandtl number Pr = 0.733,  $\gamma = 0$  and  $\lambda = 0$ .

# **RESULTS AND DISCUSSION**

The main objective of the present study is to analyze the effect of transverse conduction variation due to temperature on free convective flow along a vertical flat plate with thermal conductivity. In this simulation the values of the Prandtl number Pr are considered to be 0.733, 1.00, 1.50, 2.00 and 2.50 that corresponds to hydrogen, steam, water, methyl chloride and sulfur dioxide respectively.



Figure 2. (a) Velocity and (b) Temperature profiles for different values of  $\gamma$  with Pr = 0.733 and  $\lambda = 1.0$ .

The velocity and the temperature profiles obtained from the solutions of equations (12) and (13) are depicted in Figures 2 to 4. Also the local skin friction and the surface temperature obtained from the solutions of equations (16) and (17) are depicted in Figs 5 to 7. Numerical computation are carried out for a range of thermal conductivity variation parameter  $\gamma = 0.01$ , 0.10, 0.20, 0.30, 0.40 and transverse conduction variation parameter  $\lambda = 0.30, 0.50, 0.70, 1.00, 1.30$ .



Figure 3. (a) Velocity and (b) Temperature profiles for different values of *Pr* with  $\gamma = 0.01$  and  $\lambda = 0.3$ .

The effect of thermal conductivity variation parameter  $\gamma$  for fluid on the velocity and temperature profiles against  $\eta$  within the boundary layer with Pr =0.733 and  $\lambda = 1.00$  are shown in Fig. 2(a) and 2(b), respectively. It is seen from Fig. 2(a) and 2(b) that the velocity and temperature increase within the boundary layer with the increasing values of $\gamma$ . It means that the velocity boundary layer and the thermal boundary layer thickness expand for large values of $\gamma$ .

Fig. 3(a) and 3(b) illustrate the velocity and temperature profiles against  $\eta$  for different values of Prandtl number Pr with  $\gamma = 0.01$  and  $\lambda = 0.30$ . From Fig. 3(a), it can be observed that the velocity decreases as well as its position moves toward the interface with the increasing Pr. From Fig. 3(b), it is seen that the temperature profiles shift downward with the increasing values of Pr.

In Figs 4(a) and 4(b) describe the velocity and temperature profiles against  $\eta$  for different values of

transverse conduction variation parameter  $\lambda$  with  $\gamma = 0.01$  and Pr = 0.733. From Fig. 4(a), it can be observed that the velocity increases as well as its position moves outward the interface with the increasing values of  $\lambda$ . From Fig. 4(b), it is seen that the temperature profiles also the same as increasing within the boundary layer. It means that the velocity boundary layer and the thermal boundary layer thickness increase for large values of  $\lambda$  from 0.30 to 1.30. There is an inverse trend visible in velocity profiles.



Figure 4. (a) Velocity and (b) Temperature profiles for different values of  $\lambda$  with  $\gamma = 0.01$  and Pr = 0.733.

If we compare the velocity and temperature for the three parameters we find the velocity boundary layer and the thermal boundary layer thickness are much more clear and large for Pr and  $\lambda$  but thin for  $\gamma$ .

Figure 5(a) and Figure 5(b) illustrate the effect of the thermal conductivity variation parameter on the skin friction coefficient  $C_{fx}$  and surface temperature  $\theta(x, 0)$  against x with Pr = 0.733 and  $\lambda = 1.00$ . It is seen from Figure 5(a) that the skin friction increases monotonically along the upward direction of the plate for a particular value of  $\gamma$ . It is also seen that the local skin friction coefficient increases for the increasing values of  $\gamma$ . From Figure 5(b), it can be seen that the surface temperature increases due to the increasing value along the positive x direction for a particular  $\gamma$ .

Figure 6(a) and Figure 6(b) deal with the effect of Prandtl number *Pr* on the local skin friction and surface temperature against *x* with  $\gamma = 0.01$  and  $\lambda = 0.30$ . It can

be observed from Figure 6(a) that the skin friction decreases monotonically for a particular value of Pr. It can also be noted that the skin friction decreases for the increasing values of Pr. From Figure 6(b), it can be seen that the surface temperature distribution decreases due to the increases along the positive x direction for a particular value of Pr.



Figure 5. (a) Local skin friction coefficient and (b) Surface temperature distribution for different values of  $\gamma$  with Pr = 0.733 and  $\lambda = 1.0$ .

The variation of the local skin friction coefficient  $C_{fx}$ and surface temperature distribution  $\theta(x,0)$  for different values of  $\lambda$  with  $\gamma = 0.01$  and Pr = 0.733 at different positions are illustrated in Figures 7(a) and 7(b), respectively. It can also be noted from Figure 7(a) that the skin friction increases monotonically for a particular value of  $\lambda$ . Again Figure 7(b) shows that the surface temperature  $\theta(x,0)$  increases for increasing values of  $\lambda$ .

In compare with skin friction for the thermal conductivity variation, Prandtl number and transverse conduction variation parameters we find this is very much clear and larger for $\lambda$ . The skin friction for  $\gamma$  is clearly opposite trend with Pr and $\lambda$ . But in surface temperature we see $\gamma$  and Pr acts inversely with $\lambda$ . The effect is very clear and larger for $\lambda$ .



Figure 6. (a) Skin friction and (b) Surface temperature for different values of Pr with  $\gamma = 0.01$  and  $\lambda = 0.3$ .



Figure 7. (a) Skin friction and (b) Surface temperature for different values of  $\lambda$  with  $\gamma = 0.01$  and Pr = 0.733.

# CONCLUSIONS

The effects of thermal conductivity of fluid on free convective flow along a vertical flat plate with transverse conduction variation have been studied in this paper. From the present investigation the following conclusions may be drawn

- The velocity within the boundary layer increases for increasing values of γ and decreases for increasing values of Pr and λ.
- Significant effect is found in velocity for transverse conduction variation parameter. An inverse trend is noted in velocity profile.
- The temperature within the boundary layer increases for increasing values of  $\gamma$  and decreases for increasing values of Pr and  $\lambda$ .
- The local skin friction decreases for the increasing values of *Pr* and λ. On the other hand, this increases for increasing values of γ. Remarkable effect is found in skin friction for λ.
- An increase in the values of γ and Pr leads to an increase in surface temperature. On the other hand, this decrease for increasing values of λ. Important effect is found in surface temperature for λ. The surface temperature for λ is opposite trend with γ and Pr, which is mentionable.

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