

Structural and Mechanical Strength of Proton Radiation Processed Polyethylene Terephthalate

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Abstract

The change in structural and mechanical behavior of polyethylene terephthalate (PET) due to 2.4 MeV proton has been studied. Radiation processing of PET polymer is carried out using different low doses such as 0.2, 2.0, and 20 kGy. The Physics of microstrain and radiation-induced mesophase formation are analysed. X-ray investigation indicates that proton-induced structural modification takes place in the material. Apart from usual diffraction peaks, a low intensity broad peak is observed at small angle of about $2\theta = 10^\circ$, when the fibre axis is mounted parallel to the X-ray direction. Such peak is absent in the diffraction spectrum when the fibre axis is mounted perpendicular to the beam direction. The appearance of the extra peak in a particular orientation confirms that, the phase is 2-dimensionally oriented (mesophase). The Young's modulus (Y) of this irradiated PET sample is found to be more than that of the virgin sample with the highest value recorded for a dose of 2.0 kGy. The decrease in Y for higher dose (20 kGy) may be due to enhanced ion-induced microstrain in the sample, causing degradation in mechanical strength.

Keywords: Mesophase; Proton dose; Young's modulus; Microstrain.

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1. Introduction

In semi-crystalline polymers normally two phases exist namely crystalline and amorphous. But another phase is detected in the same polymer, when it is quenched from the melt [1]. This third phase of the polymer is called the mesomorphic phase or

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the mesophase which is intermediate between the crystalline and amorphous phase. It is a state of matter in which the degree of molecular order is intermediate between that of the perfect three dimensional, crystalline solids and that of the amorphous state. The study is important because, the mesomorphic phase has a reinforcement effect on the whole polymer matrix that leads to an increase in hardness with annealing of the oriented polymer [2]. Again, from the technological point of view, as the mesophase has proved impermeable to vapours at low activity, behaving like the crystalline phase, so the possibility of improving the impermeability of polyethylene terephthalate (PET) need to be explored for many applications [3,4].

Existence of mesophase in polymers like PET, and polypropylene were confirmed using X-ray diffraction [5,6], solvent absorption [7], FT-Raman scattering [5], and nuclear magnetic resonance techniques [8] by various authors. However, proton-induced mesophase formation is a very recent work reported by Sahoo *et al.* [9,10].

In the present work, mesomorphic phase structure has been formed in the PET material by radiation heating process. The effect of fibre structure and its orientation due to different mounting have been studied using X-ray diffraction technique. The change in mechanical behavior of the fibre has also been studied due to formation of mesophase and total ion beam (IB) induced microstrain developed in the fibre using Instron technique. The study of MeV ion-induced modified polymer is very much interesting and important from technological point of view [11]. It is also observed that, the modification of polymer properties under ionizing radiation is a field of great interest due to its increasing uses in various fields [12,13]. Ionizing radiation can change the macroscopic properties and the molecular structure of polymeric materials [14]. The irradiated polymer possesses improved tensile strength, increased rigidity, improved yield strength, higher melting temperature and swelling in the usual solvent.

2. Experimental

2.1. PET material

PET material in the form of fibre used in the study was collected from a commercially available polyester plant. The molecular weight of repeated unit or monomer of PET is 192 g/mole/unit mer and having weight average molecular weight 25,330 (*i.e.*, $\overline{M}_w = 25,330$).

The three major processes used for the production of above PET fibre are esterification, polycondensation and spinning. In esterification process, mixture of purified terephthalic acid and ethylene glycol were used to produce oligomer. The above produced oligomer was passed through a 3-stage polycondensation reactor under various machine-setting parameters to produce viscous PET polymer. The above viscous polymer molten was again passed through a spinneret of very fine holes. While leaving the holes, the viscous material formed wire, which when passing through a heater and hot air produced long fibre filaments.

2.2. Proton irradiation

A proton beam of energy 2.4 MeV was obtained from the 9SDH-2, “National Electrostatic Corporation, USA make 3MV horizontal tandem type pelletron accelerator,” to carry out ion irradiation in air. The PET fibre material was irradiated for three different low doses such as 0.2 kGy, 2 kGy and 20 kGy at normal temperature and pressure in air. The amounts of charge trapped in the material for the above irradiations are 0.0048 μC , 0.048 μC and 0.48 μC respectively. The beam was initially collimated by a graphite collimator to a beam size of 3 mm diameter and was extracted into air using a KaptonTM foil of 8 micron at the exit point of the vacuum (1×10^{-6} mbar) chamber. The diameter of the external proton beam may be increased up to 10-15 mm circular patch by proper adjustment. The external beam current measurement was performed using a rotating vane chopper designed at the Institute (Institute of Physics, Bhubaneswar). In the present study, initially 3 MeV proton beam was allowed to travel 3 cm in air inside the irradiation cell (an aluminum cylinder of 15 mm diameter and 30 mm length) rotating with 1 Hz frequency for homogeneous irradiation, during which the energy of the proton beam gets reduced to 2.4 MeV before interaction with the material.

2.3. Sample Preparation

The PET sample was mounted on a typical sample holder to form a flat sample of uniform length, breadth, thickness and well-parallelized bundle of filaments in each test sample for X-ray diffraction (XRD) investigation.

Furthermore, for the investigation of mechanical behavior, strips from the general-purpose brown paper of area $80 \times 30 \text{ mm}^2$ have been taken. From the center of the strip, a $20 \times 20 \text{ mm}^2$ patch was taken out. Fibre of length 80 mm was initially fixed at the center of paper strip with the help of a suitable adhesive, which is non-reactive to the fibre. Again, another paper strip of the same type was fixed on the top of the fibre, so that the fibre should sit properly at the center of both the paper strips. The well-mounted dried sample was used for Instron study.

2.4. Characterization

We have carried out X-ray diffraction applying two orientation sample mounting procedure using “Rigaku Ultima-IV”, X-ray diffractometer. As our interest is on mesophase analysis of PET sample, we preferred to mount the sample in two different ways, one is putting the fibre axis perpendicular to the beam direction and the other is putting it parallel to the beam direction. The X-ray diffraction patterns were recorded with a step size of 0.02° on a 5° - 50° range with a scanning rate of $0.34^\circ/\text{s}$. Line focus CuK_α -radiation from an X-ray tube (operated at 40 kV and 40 mA) was collimated through Soller slit (SS) of 5° , fixed divergence slit of 0.67° and mask (8 mm), before

getting it diffracted from the sample. A D/teX ultra-high-speed position sensitive detector was mounted on the arm of the goniometer circle of radius 285 mm to receive diffracted X-ray signal, and analyzed using the integrated X-ray powder diffraction software PDXL 2.7.

The instrument used to study the tensile properties of PET fibre materials was a kni UTM-201, electronic textile-testing machine which is commonly known as Instron (Kamal Metal Industries, India). Two numbers of strips from each PET polymer sample have been tested to find the average values of the mechanical parameters. The gauge length (mm) for the test sample was taken to be 20 mm. The load cell (kg) was taken as 50 with load sensitivity of 0.2. The test speed (mm/min) selected was 10, however the maximum speed was set at 50 mm/min. The elongation least count was set at 0.025 mm.

3. Results and Discussion

3.1. IB Dose analysis

The irradiated polymers is observed to possess mesophase which is improved compared to the 'virgin' material. The ratio of crosslinking and degradation depends on the chemical structure of a polymer and it is usually appraised by the radiation-chemical yield or G -value of crosslinking which is defined as the number of chemical reactions or events occurs in the absorption of 100 eV of radiation energy. For PET, the weight average molecular weight \overline{M}_w and the radiation chemical yield $G(X)$ are given as 25,330 and 0.08 respectively [15,16].

Hence, the dose required to convert maximum radiation-induced crosslink molecules in the above PET sample can be defined theoretically as:

$D_{rad} = 9.65 \times 10^6 / G(X) \overline{M}_w$. Using the values of $G(X)$ and \overline{M}_w , $D_{rad} = 4.768 \times 10^3$ kGy.

Again, the ion dose in terms of specific energy loss $\left(\frac{dE}{dx}\right)$ or stopping power and

fluence F can be defined as $D_{rad} = \left(\frac{dE}{dx}\right) F$. The value of $\left(\frac{dE}{dx}\right)$ for 2.4 MeV proton in

PET material is 1.864×10^8 eV/cm ($1\text{Gy} = 1\text{J/kg} = 6.289 \times 10^{18}$ eV/kg = 8.786×10^{15} eV/cm³). Hence, the ion-dose in terms of gray (Gy) can be calculated using the above

conversion factor for the PET solid as $D_{rad} = \frac{(1.864 \times 10^8 \text{ eV / cm}) \times F}{8.786 \times 10^{15} \text{ eV / cm}^3}$. So, for a fluence

of 1×10^{10} p/cm² in the present case, $D_{rad} = 0.2122$ kGy ≈ 0.2 kGy, this is the minimum radiation dose we have taken for the modification purpose. A maximum of 20 kGy dose was used to modify the sample.

3.2. XRD analysis

The PET fibre is mounted in two different orientations i.e., the X-ray beam parallel to the fibre axis, and the X-ray beam perpendicular to the fibre axis. The results are shown in the Fig. 1.

It is observed that, there is no distinct variation in d -spacing in either case of the mountings. Apart from the usual peaks, a low intensity broad extra peak is observed in the spectrum A (fibre axis parallel to the beam direction) of all cases of the fibres at small angles about $2\theta = 10^\circ$ as shown in Fig. 2 (extended version of a part of Fig. 1). Nonetheless, it is absent in the spectrum B (fibre axis perpendicular to the beam direction). This is implicative of the fact that when the fibre axis is parallel to the beam direction, nearly all the atoms of the oblique planes of the fibre helix participate in the diffraction. As a result, the 2-dimensionally ordered system formed by the atoms of the fibre helix produces prominent diffraction peaks owing to constructive interference of waves (mesophase). On the other hand, when the fibre axis is perpendicular to the beam direction, scattering from the mesophase does not produce prominent peaks because the effects are mutually cancelled out due to irregular distribution. The common peaks in both cases of the mounting indicate that the phases are 3-dimensionally arranged. However the extra peak (mesophase) found in one orientation and not in other confirmed that, the given phase is 2-dimensionally oriented.

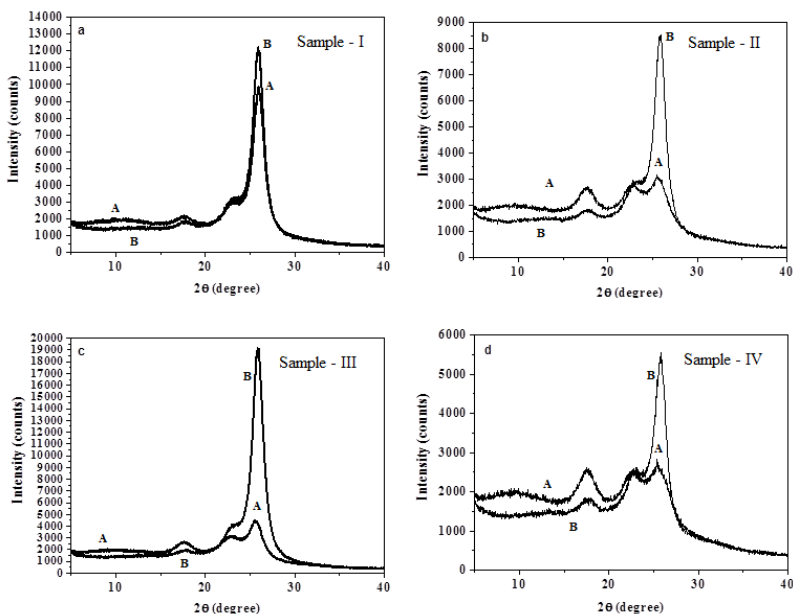


Fig. 1. X-ray diffraction pattern of PET fibre when the fibre axis is Parallel [A], and perpendicular [B] to the X-ray beam, (a) virgin sample, (b) sample irradiated at a dose 0.2 kGy, (c) sample irradiated at a dose 2 kGy, and (d) sample irradiated at a dose 20 kGy.

The microstrain has been estimated using $\varepsilon = \frac{\Delta d}{d} = \left(\frac{d_s - d_u}{d_u} \right)$, where d_s and d_u are the spacing in the irradiated (stressed) and non-irradiated (unstressed) fibres respectively. The value of total microstrain was calculated using the XRD data as shown in the Table 1. Among all the irradiated samples, the least value of total microstrain is developed in sample-III, which is found to be 0.055. The highest value of total microstrain is found to be 0.135 in sample-IV. This maximum value of total ion-induced microstrain in sample-IV causes more degradation and less crosslink as compared to sample-III. The mesophase peaks of all the irradiated samples are observed to be shifted to the lower angles than the virgin, which is due to the ion-induced microstrain developed in the 2D-oriented surface of irradiated fibre.

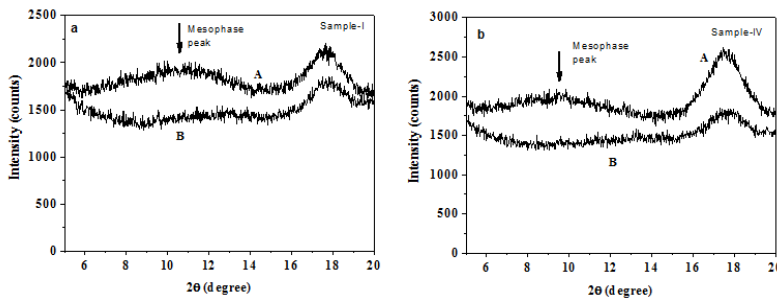


Fig. 2. Mesophase peak in the (a) virgin, and (b) sample irradiated at the highest dose.

Table 1. Microstrain by X-ray diffraction (Parallel mounting).

Sample	2θ (deg.)	I_p (cps)	d (Å)	Δd	$\varepsilon = \Delta d/d$	Total ε	% C
I	10.27	1942	8.606	-	-		51.2
	17.56	2122	5.048	-	-		
	23.10	2930	3.848	-	-		
	25.97	9809	3.429	-	-		
II	9.14	1994	9.671	1.065	0.12	0.128	40.3
	17.56	2623	5.048	-	-		
	22.79	2714	3.899	0.051	0.01		
	25.53	3066	3.486	0.057	0.017		
III	9.84	1943	8.982	0.376	0.04	0.055	45.6
	17.64	2667	5.025	-0.023	-0.004		
	22.84	3063	3.890	0.042	0.01		
	25.70	4223	3.463	0.034	0.009		
IV	9.41	2011	9.394	0.788	0.09	0.135	41.7
	17.47	2540	5.073	0.025	0.005		
	22.63	2516	3.926	0.078	0.02		
	25.45	2743	3.498	0.069	0.02		

Again, the percent crystallinity %C has been calculated using the relation $\%C = (A_{cryst} / A_{total}) \times 100$, where A_{cryst} and A_{total} are total area of crystalline peaks and the diffraction pattern respectively. Percent crystallinity of virgin fibre has been

found to be 51.2%. However, the percent crystallinity of samples irradiated at different low doses were found to be less than the virgin sample. This is mainly because of the degradation of polymer and formation of proton-induced mesophase.

3.3. Instron analysis

Tensile properties of polymer are very important to understand the mechanical behavior. Radiation dose plays an important role for the modification of tensile strength and modulus of elasticity of polymer [17]. The Young's modulus or tensile modulus, which is a function of ultimate tensile strength (*UTS*) of the material has been estimated using the relation, $Y = \frac{UTS}{\varepsilon^{Corr}}$, where $\varepsilon^{Corr} (= k\varepsilon)$, k is the correction

factor and ε is the engineering strain) is the corrected strain. Mechanical strength of the virgin and irradiated PET samples of fibre cross section area 0.625 mm^2 can be analysed using Instron from the plots related to elongation *versus* load as shown in the Fig. 3. The various important parameters obtained experimentally are given in Table 2.

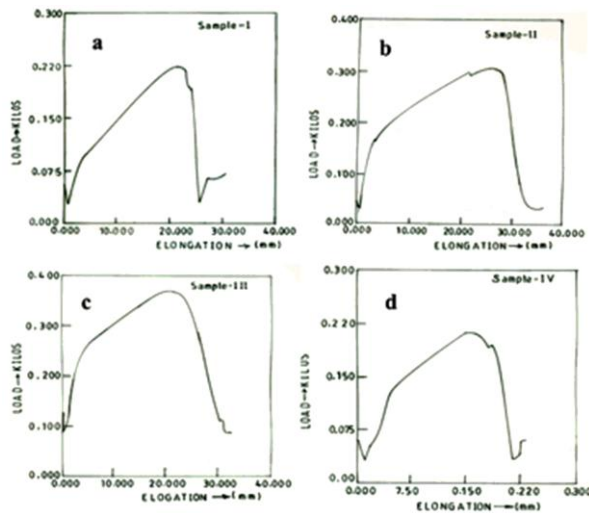


Fig. 3. Elongation *versus* load: (a) virgin sample, (b) sample irradiated at a dose 0.2 kGy, (c) sample irradiated at a dose 2 kGy and (d) sample irradiated at a dose 20 kGy.

The Young's modulus (Y) of virgin fibre is found to be 19.295 GPa. It is observed that the Y value increases with increase in proton dose upto 2 kGy (sample-III) and thereafter it decreases. But in any case it is found to be more than the virgin sample as shown in the Table 2. The highest value of Y recorded is 38.425 GPa in sample-III. Such observation is possibly due to lower value of radiation induced microstrain, that causes maximum crosslinking of molecules (as confirmed from the XRD). The decreased values of Y (23.54 GPa) in case of fibre sample-IV (20 kGy) may be due to the formation of excessive ion-induced microstrain, which causes reduced crosslink

and increased degradation as compared to sample-III (2 kGy). Higher value of the microstrain causes degradation in the mechanical strength of the fibre sample.

Table 2. Mechanical parameters of PET material.

Sample	Dose (kGy)	Max. load (kg)	Elongation at max. load (mm)	% Elongation		UTS (MPa)	ϵ^{corr}	Y (GPa)	Y _{avg.} (GPa)
				at max. load	at break				
I	0	0.4000	15.98	79.88	134.75	62.78	0.003	20.93	19.295
		0.3375	17.68	88.38	135.15	52.97	0.003	17.66	
II	0.2	0.3688	20.23	101.13	165.74	57.88	0.002	28.94	29.92
		0.3938	23.27	116.37	180.62	61.80	0.002	30.9	
III	2	0.4625	19.35	96.75	162.22	72.60	0.002	36.3	38.425
		0.3875	14.18	70.88	123.28	60.82	0.002	40.55	
IV	20	0.3063	14.95	74.75	114.61	48.06	0.002	24.03	23.54
		0.2938	20.43	102.13	175.78	46.10	0.002	23.05	

4. Conclusion

Proton-induced mesophase formation in the PET polymer has been investigated with three different proton doses of irradiation. Structural change in the PET sample is analysed using XRD technique both at parallel and perpendicular mountings of the sample axis with respect to the X-ray beam. The common peaks in both the mounting indicated that the phases are 3-dimensionally arranged. However the extra peak (mesophase) found in parallel mounting confirmed that, the phase is 2-dimensionally oriented. The mesophase peak of all the irradiated samples is observed to shift towards the lower angles compared to the virgin sample, which might be due to the ion-induced microstrain developed in the 2D-oriented surface of the irradiated fibre. The effect of ion-induced microstrain on mechanical strength is studied using the Instron technique. The Young's modulus (Y) of all the irradiated samples are found to be more than that of the virgin sample. The present investigation will contribute greatly towards the study of mechanical strength of ion beam irradiated polymer materials and to understand various physical parameters of the materials.

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