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Quality-by-Design Approach and Optimization of Risk Factors by Box-Behnken Design in Formulation Development of Aspirin and Glycine Orally Disintegrating Tablet

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Abstract

Quality-by-design approach (QbD) was applied to develop an orally disintegrating tablet (ODT) formulation of aspirin and glycine. At first, the target quality profile and critical quality attributes (CQAs) of the product were identified. Risk assessment was accomplished by failure mode and effects analysis (FMEA) method to assess the factors having a significant effect on CQAs like disintegration time (DT), friability and assay of aspirin and glycine. Low substituted hydroxypropyl cellulose (L-HPC), croscarmellose sodium (CCS) and punch-diameter were found critical for DT and friability. The box-Behnken design was applied to optimize those 3 factors to reach a target DT of \leq 30 sec. It was found that a punch-diameter between 8.7 ~ 9.3 mm, CCS in a range of 4 % ~ 5 %, and L-HPC in a range of 2 % ~ 8 % produced the best oral disintegrating property and reduced the risk. In summary, this work represented an excellent example of the application of QbD approach in ODT formulation development.

Keywords: Aspirin; Glycine; Risk assessment; Quality-by-design; Box-Behnken design.

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1. Introduction

Acetylsalicylic acid, commonly known as Aspirin (ASP), acts as a platelet aggregation inhibitor. There are plenty of studies that indicate the fact that ASP at low dose (50 - 320 mg/day) acts as an effective antithrombotic agent [1]. Thus, it reduces the incidence of myocardial infarction and death in patients with unstable angina [2]. Glycine (GLY) is an essential amino acid that has been proven to reduce gastric irritation of ASP when it is given concurrently with ASP [3,4]. It was also studied that GLY improves the solubility of ASP in water and also masks the sour taste of ASP to some extent when it is disintegrated on tong [5,6]. Consequently, ASP and GLY now a day comes up in combination as orally disintegrating tablet (ODT) in different strength (e.g., ASP 75 mg + GLY 37.5 mg, ASP 100 mg + GLY 45 mg etc.). ODTs have gained much interest during

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the last decade due mainly to their ease of administration in patients with deglutition disorder [7-10]. Formulation of ODTs, however, has always been a great challenge as many factors can stifle the successful development of ODTs. Among those factors, taste masking of drug substance, quick disintegration time, low tablet weight, small tablet dimension, enough mechanical strength, physical stability throughout the shelf life are few to mention [8,11].

In the current study, we put effort to develop a formulation of the orally disintegrating tablet of ASP 100mg and GLY 45mg by quality by design (QbD) approach following the ICH Q8 guideline. To do so, we first set the target quality profile of the product. This includes the physical and chemical attributes to meet the safety, efficacy and patient compliances for the ODT of ASP and GLY combination. Then we identified the critical quality attributes (CQA) that are needed to be within a certain limit or range to achieve the target quality. After that, through extensive literature review and justification, we selected the excipients appropriate for the current formulation development. We performed a quantitative risk assessment of the selected excipients and process parameters through the failure modes and effects analysis (FMEA) method to identify the risk factors among the excipients and process parameters that are most critical to achieving the CQAs. Last but not least, we optimized the high-risk factors (critical excipients and/or process parameters) through the design of experiments (DoE) and statistical analysis [12,13]. We applied Box-Behnken design, a type of response surface methodology (RSM) in the DoE. The developed formula also underwent a stability study to assess its chemical and physical stability throughout the shelf life.

We performed an extensive literature search for any report of ASP and GLY combination tablet in either ODT or immediate-release form, but to the best of our search, there is none. The current work is, therefore, a thorough guide and reference for the development of ODT of a combination of these two therapeutic agents in the treatment of heart disease.

2. Materials and Methods

2.1. Materials

Aspirin (potency 99.3 %), Glycine, L-HPC, CCS, microcrystalline cellulose (Type 101), pregelatinized starch, purified talc, and colloidal silicon dioxide (Aerosil-200) were a kind gift from Beximco Pharmaceuticals Limited, Bangladesh.

2.2. Equipment

Such equipment as a calibrated weighing machine (Radwag, Poland), 30 mesh screen, 8station compression machine (Proton Electronics, India), calibrated hardness tester (YD1, China), disintegration tester (Electrolab, India) located in the Pharmaceutical Technology lab of the University of Dhaka were used in the experiment. Accelerated stability study was conducted in Clima Cell Stability Chamber (Model: CLC-B2V/CLC-404, Year: 2001, manufactured by BMT Medical Technology).

2.3. Elements of quality-by-design (QbD)

According to ICH Q8 guideline, the quality by design approach for pharmaceutical formulation development includes such elements as quality target product profile (QTPP), critical quality attributes (CQA), identifying risk factors (drug substance, excipients and process attributes) that can have a potential effect on CQAs, optimization of risk factors by the design of experiments (DoE) and statistical analysis, and create design space to minimize the risks.

2.3.1. *Quality target product profile (QTPP)*

This is a description of all of the physiochemical attributes of the products that are needed to achieve for safety and efficacy of the ultimate product during its shelf-life on the market. QTPP elements that are typically taken into consideration are the route of administration, dosage form, dosage strength, pharmacokinetic targets, physical and chemical properties of drug substance (e.g., crystallinity, particle size distribution, salt form, etc.) and drug product (e.g., friability, dissolution, disintegration time, assay etc.), microbiology, container closing system, shelf-life, etc.

2.3.2. Critical quality attributes (CQA)

These are those elements of QTPP that are needed to be within a certain limit for the efficacy and safety of the product. For example, ODT tablets should disintegrate less than 30 sec, an assay of a drug substance should be within ± 10 % of its claim, etc.

2.3.3. Risk factors

Drug substance properties, excipients and the process parameters that have a potential effect on CQA, meaning CQA can change significantly as a function of those factors.

2.3.4. Risk assessment

Initial risk assessment (qualitative) is done from previous experiences, pilot studies, literatures and references. Then, the quantitative risk of each selected excipient and process parameters is assessed by FMEA method.

2.3.5. Design of experiments (DoE)

From the risk assessment study, selected high-risk factors are subjected to optimization in a systematic way to find out their effect and interaction effects on the response. Depending upon the number of variables (i.e., the number of risk factors), different types of experiments can be applied for optimization. Scientists can choose any of the numbers of experimental designs for optimization, but there are some preferences with a number of variables to keep the number of experimental runs as few as possible. For example, if two variables are needed to be optimized, then a full factorial design with a center point is preferred. In such a case, a total 5 runs are required. But it is advisable to make three replicates at the center point leading to 7 runs in total. The Center point measures the curvature effect in the factor-response relationship. If the curvature effect is significant as indicated by the p-value, then the experiment should be augmented to response surface methodology (RSM). In such a case, another four experiments would be required, meaning 11 runs in total. If three factors are optimized simultaneously, then RSM is better than factorial design in terms of fewer runs and better prediction. For the three factors optimization experiment, Box-Behnken RSM (17 runs with 5 replicates at center point) is preferred to Central Composite RSM (20 runs with 5 replicates at center point). Four and five factors can be optimized by resolution IV and resolution V design which are nothing but fractional factorial designs.

2.3.6. Statistical analysis [14]

Analysis of Variance (ANOVA) is performed to calculate different statistical parameters like F-value, p-value, the sum of squares, degree of freedom, etc. Among those parameters, the p-value is the most important tool to the formulation scientist. p-value indicates whether or not the null hypothesis holds good. A p-value greater than 0.05 (or sometimes 0.1) indicates that the null hypothesis is true i.e., the experimental factors have no significant effect/influence on the response. A p-value less than 0.05 indicates the null hypothesis is rejected, i.e., factors substantially affect the response. As an important part of ANOVA, examination of residuals is accomplished. Examination of residuals indicates whether the model is adequate or not adequate.

Regression analysis is another important step in the DoE. In regression analysis, the relationship between independent variables and response is characterized quantitatively by a mathematical model. Such parameters as determination coefficient (R^2), adjusted determination coefficient (Adj- R^2), predicted determination coefficient (Pred- R^2) are usually examined.

2.3.7. Design space

It describes the functional relationship between the risk factors and the CQAs. In a practical sense, design space gives a certain range or limit of critical excipients or process parameters within which CQAs meet their target. In other words, design space describes the range of risk factors within which the risk of impacting the CQAs is minimized or diminished.

2.4. Software

The trial version of Design-Expert software (Design-Expert 10.0.8) was used to analyze the ANOVA and other statistics.

3. Results and Discussion

3.1. Quality target product profile (QTPP)

A brief target quality profile was set upon the definition of ODTs given by FDA as 'A solid dosage form containing medicinal substances which disintegrate rapidly, usually within a matter of sec, when placed upon the tongue'. FDA specified the in vitro disintegration time of ODT equal to or less than 30 sec. FDA also recommends the tablet weight be equal to or less than 500 mg. Based upon the description and recommendation of US-FDA guidance for ODT, the QTPP of current formulation development was set as shown in Table 1.

Quality Attributes	Target
Route of Administration	Oral; intended to place on tongue and dissolve on tongue in a matter of sec.
Disintegration Time	<i>in vitro</i> disintegration time of approximately 30 sec or less, using United States Pharmacopeia disintegration test.
Tablet Weight	Weight should be less than 500 mg. In the current study target tablet weight was 220 mg.
Mechanical Strength	Sufficient to ensure physical integrity during manufacturing, packaging, shipment and patients' handling. A friability of not more than 1.0 % would be considered to meet this target at the development stage.
Physical Stability	Physical integrity throughout the accelerated stability for 6 months. Physical integrity would typically include retaining hardness, appearance throughout the shelf life.
Taste and Smell	Should have acceptable taste and smell throughout the shelf life.
Chemical Stability	Assay of ASP and GLY not less than 90 % of initial estimation after 6 months' accelerated stability would be considered to meet chemical stability.
Container	Qualified container closing system that provides best protection against moisture. Aluminum blister or High-Density Polyethylene (HDPE) containers with moisture absorbent are best in this class.

Table 1. Quality target product profile of ASP and GLY orally disintegrating tablet.

3.2. Critical quality attributes (CQA)

In the current study, disintegrating time (DT), friability and assay of ASP and GLY were considered the CQA. ODTs are intended to disintegrate on the tongue within sec without any effort of chewing or aid of liquids. Therefore, rapid disintegration on the tongue is a CQA for ODT. To meet the rapid disintegration, ODTs are often manufactured with a high amount of super-disintegrating agents and with low hardness, often resulting in low physical integrity. Friability is an important indicator of physical integrity and is another

CQA in the current case. If tablets are of low physical integrity, then they may break down during processing, transportation and handling, leading to safety and efficacy issues. There should be a balance between hardness and friability. ODTs should be manufactured with the lowest possible hardness while ensuring acceptable friability during the shelf life. A friability of not more than 1 % was set as a target. Aspirin is a well-studied molecule and it has been shown to be a moisture sensitive and heat-labile molecule. Both moisture and heat facilitate its degradation to salicylic acid and acetic acid. Consequently, an assay of aspirin is an important CQA in this case. Assay of aspirin and glycine would be ensured more than or equal to 90 % throughout the stability study.

3.3. Basic formulation elements

Basic elements of ODT tablet formulation and possible options for current development were presented in Table 2.

Functional Category	Available options of commonly used excipients					
Filler or Diluent	Microcrystalline cellulose, Starch, Lactose, Pregelatinized Starch,					
	Mannitol, Dibasic calcium phosphate					
Binder	Povidone, Copovidone, Hydroxy Propyl Methyl Cellulose, Hydroxy					
	Propyl Cellulose, Low substituted HPC, Starch					
Super-disintegrant	Sodium Starch Glycolate, Croscarmellose sodium, Crospovidone,					
Lubricant	Magnesium stearate, Stearic acid, Purified talc, Calcium stearate,					
	Sodium stearyl fumarate etc.					
Glidant	Colloidal silicon dioxide					

Table 2.	Basic elements	of ODT formulation	and common	excipients.
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3.4. Excipients selection by qualitative risk assessment

In the quality by design, appropriate excipient selection in terms of compatibility with the drug molecule is of prime concern before the development trial. In the current study, a thorough literature search was done to find out those excipients that are best for the ODT formulation and are compatible with ASP. The selection of excipients for each category was properly justified.

3.4.1. *Filler*

Starch is a good filler with the disintegrating property but possesses poor flow property and contains a high amount of free moisture, which can facilitate hydrolysis of ASP. Native starch can be replaced by pregelatinized starch (starch 1500) which has a good flow. The high moisture content of starch 1500 could be a threat to the stability of ASP; however, literature shows that water activity is low for starch 1500 compared to other commonly used fillers, which is why starch 1500 produces ASP tablet with better stability [15,16]. Dibasic calcium phosphate could be a better choice, but it is abrasive in nature and needs a higher amount of magnesium stearate (at least 1 %) to avoid sticking during ejection [17]. Magnesium stearate, on the other hand, is incompatible with ASP [18-22].

Anhydrous lactose is a good choice for direct compression (DC) tablets, but some studies showed that it might not be a better choice in ODT as it hinders the disintegration [23-26]. Lactose monohydrate, on the contrary, aid in disintegration but its use can be limited by its moisture content and water activity which could facilitate ASP degradation [15]. In the case of microcrystalline cellulose (MCC) both moisture content and water activity are low [15]. Numerous studies prove that MCC is a binder, diluent, disintegrant, and also has some self-lubricating property [17]. MCC is broadly regarded as the filler having the best binding properties in the dry state [27]. In addition to its dry binding property also acts as a disintegrating agent due to its swelling property [25,28]. Upon this review, MCC was primarily chosen as filler during the optimization trials.

3.4.2. Binder

Among those binder stated in Table 1, L-HPC was best due to such facts as its dry binding capacity with anti-capping property and, more importantly, its swelling capacity which aids in disintegration [17]. L-HPC is the binder of choice in orally disintegrating tablets functioning as both binder and disintegrating agents [29,30].

3.4.3. Super-disintegrating agent

Disintegrating property does vary depending upon the API characteristics. Zhao and Augsburger carried out an experiment to prove that croscarmellose sodium (CCS) was most effective for reducing disintegration and improving dissolution of ASP among the three super-disintegrants [31,32]. Consequently, CCS was considered as the super-disintegrant in the current study.

3.4.4. Lubricant and glidant

Salts of stearates (magnesium stearate, calcium stearate, etc.) have ever been the most effective lubricant, but numerous studies proved that stearate salts react with ASP resulting in degradation of ASP into salicylic acid and acetic acid [18-22]. Many studies investigated the stability of ASP with talc and got better results [33-35]. Consequently, talc was chosen as a lubricant. Colloidal silicon dioxide was only one choice as a glidant.

3.5. Quantitative risk assessment by FMEA

Following the literature review, most compatible and convenient excipients that would best serve the QTPP of current development were chosen. Then the risk of each excipient on the major CQA of interest (i.e., DT) was quantitatively assessed by FMEA method. Risk assessment was done with respect to the probability of each excipient impacting DT, the degree of severity of impact and the detectability of impact. Scoring of the probability, severity and detectability was explained in Table 3.

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Score	Probability of Impacting	Severity	Detectability
1	Extremely low chance of impacting CQA, never happens usually	No impact on CQA	Detectable in unit operation
2	Low chance of impacting, but may happen	Some impact, but reversible	Detectable after the unit operation and before end product testing
3	Moderate chance of impacting and frequently happens	Moderate Impact but not quality threatening	Detectable only at end product testing
4	High chance of impacting and always happens	High impact and irreversible	Failure can never be detected

Table 3. Explanation of risk level of different terms in FMEA.

Based upon the scoring system as stated above, quantitative risk assessment of selected excipients and process parameter was shown in the Table 4.

Excipients/ Process	Effect on DT	Probability of impacting DT	Severity of impact	Detecta -bility	RPN ¹	Risk rating ²
L-HPC	It has both binding and swelling effect.	4	3	3	36	High
Croscarmellose Sodium	Super-disintegrating agent	4	4	4	64	High
MCC-101	Diluent and also a weak disintegrant	1	1	1	1	Low
Purified Talc	Lubricant	3	3	2	18	Medium
Aerosil-200	Glidant	2	2	1	4	Low
Punch Diameter	Higher dia increases surface area and decreases the DT	4	4	3	48	High
Hardness	DT is proportionate to Hardness	4	3	1	12	Low

Table 4. Quantitative risk assessment of material attributes and process parameter on DT.

¹RPN=Risk Priority Number. ²Note:1~16 represents low risk, 17~34 medium risk and 35~64 high risk

It was found that L-HPC, CCS and Punch Diameter have got high-risk ranking. Therefore, these three components were subjected to experimental design for optimization.

3.6. Manufacturing procedure

Each formulation in the subsequent steps was manufactured by direct compression (DC). Both ASP and GLY were first milled by passing through 0.5 mm mesh. Tablet weight was fixed at 220 mg comprising such fixed weight components as 100 mg ASP, 45 mg GLY, purified talc 1.1 mg (0.5 % w/w) and colloidal silicon dioxide 1.1 mg (0.5 % w/w). L-HPC and CCS varied in each formula according to the design and total weight was adjusted with diluent (MCC-101). In the preparation of each formula, at first, ASP, GLY, CCS, L-HPC and MCC-101 were dispensed and passed through 30 mesh and then mixed thoroughly for 10 min. Then purified talc and colloidal silicon dioxide were passed

through 40 mesh and mixed with the previous mixture for 1 min. Optimization batches were compressed at 5.5 newtons (N) pressure and within a hardness of $6 \sim 7$ kilopond (Kp). To produce the same hardness, the upper punch position was adjusted, and compression thickness was changed from batch to batch.

3.7. Design of experiment for optimization

For simultaneous optimization of three-factor, a Box-Behnken design comprising 6 factorial points, 6 axial points and 5 replicates at the center point was constructed by the Design-Expert software. Experimental levels of critical factors were selected and justified based on literature and experience. Handbook of Pharmaceuticals states the usual level of CCS in tablets as $0.5 \% \sim 5 \%$ (w/w) though 2 % is enough in direct compression. But, as in the current case lowest possible DT is concerned, the experiment range was started with 2 % lower level and 6 % high level. L-HPC was tested between 2 % ~ 10 % (w/w). Punch diameter was examined between 8.0 mm to 10.0 mm. These were presented in table 5.

Experimental		Levels of fact	s of factors Response		Target of	
factors	High	Medium	Low	Response	optimization	
L-HPC (% w/w)	10	6	2	Disintegration	$DT \le 30$ sec (i.e.,	
CCS (%w/w)	6	4	2	Time	lower the better)	
Punch dia (mm)	10	9	8	Time	lower the better)	
Constant factors	Fixed	levels				
Lubrication time	1 min.					
Compression force	5.5 N					
Hardness	6~7 Kr)				
Environment	40 %~.	50 % RH, 20	°C~25 °C			

Table 5. Experimental and constant factors, response and its target.

Each trial batch was prepared and compressed according to the random standard order created by the software to avoid system biasness and reduce the effect of lurking factors if any. During manufacturing and compression, such constant factor as mixing order, lubrication time (1min), humidity (RH 40 % ~ 50 %), temperature (20 °C ~ 25 °C), compression force (5.5 N) and hardness (6~7 Kp) were maintained at a fixed range/level for all the trials. Disintegration time was determined in 750 mL water, warmed at 37 ± 0.5 °C and without a disc to create sufficient discrimination among the batches. The design layout and the measured DT were shown in Table 6.

Table 6. Design layout with randomized standard order and the response (DT).

Standard	Run	L-HPC	CCS	Punch Dia	DT
Order	Order	(% w/w)	(% w/w)	(mm)	(sec)
12	1	6	6	10	16
16	2	6	4	9	19
2	3	10	2	9	31
1	4	2	2	9	28
14	5	6	4	9	20
17	6	6	4	9	19

Standard	Run	L-HPC	CCS	Punch Dia	DT
Order	Order	(% w/w)	(% w/w)	(mm)	(sec)
13	7	6	4	9	20
3	8	2	6	9	22
15	9	6	4	9	19
6	10	10	4	8	28
11	11	6	2	10	25
7	12	2	4	10	17
10	13	6	6	8	28
8	14	10	4	10	13
5	15	2	4	8	22
9	16	6	2	8	32
4	17	10	6	9	24

3.8. Statistical analysis

ANOVA was conducted (by the Design-Expert software) to test the significance of the response surface quadratic model, which was presented in Table 7. The significance of the experimental model and each term was assessed primarily by the *p*-value and secondarily by Fisher's ratio (*F*-value). Experimental model and any term having a *p*-value <0.05 was considered statistically significant and a larger *F*-value indicates greater dispersion of response from a mean value indicating the prominent effect of factors on the response. It was found that *p*-value for the quadratic model and each main effect was less than 0.05 i.e., significant. Most of the interaction effects and square terms were also significant. Lack-of-fit was found to be insignificant (*p*-value > 0.05), meaning a good fit of the model. A large model *F*-value (149.77) also indicated the significance of the experimental model.

The polynomial regression equation for describing the correlation between the factors and response was constructed as follows:

Disintegration time (DT) = 19.40 + 0.88A - 3.25B - 4.88C - 0.25AB - 2.50AC - 1.25BC + 0.80A² + 6.05B² - 0.20C² (A=L-HPC, B=CCS, C=Punch Dia)

The quality of the regression equation was assessed by determination coefficient (R^2), adjusted determination coefficient (Adj- R^2) and predicted determination coefficient (Pred- R^2) [Table 7]. The determination coefficient (R^2) was found 0.99 indicating excellent fitting of the experimental data to the regression line. Adj- R^2 and Pred- R^2 were in reasonable agreement, i.e., the difference between them is less than 0.20. Adequate precision measures the signal-to-noise ratio and a ratio greater than 4 is desirable [14]. Here, adequate precision was found 41.05, which indicated that this model could be used to precisely navigate the design space.

		-	-	-	-	
ANOVA				Regression analysis		
Source	df	F-value	P-value	R^2	:	0.9948
Model	9	149.77	< 0.0001	Adj- R^2	:	0.9882
A: L-HPC	1	17.77	0.0041	Pred- R^2	:	0.9539
B: CCS	1	241.43	< 0.0001	Adeq-Precision	:	41.05
C: Punch	1	543.21	< 0.0001	Adj- R^2 - Pred- R^2	:	0.0343
AB	1	0.71	0.4260			
AC	1	71.43	< 0.0001			
BC	1	17.86	0.0039			
A^2	1	7.70	0.0275			
B^2	1	440.33	< 0.0001			
C^2	1	0.48	0.5102			
Lack-of-fit	3	1.39	0.3678			

Table 7. ANOVA for response surface quadratic model and regression analysis.

To check model adequacy, residuals plots were constructed. Residual plots indicate whether there is an outlier in the data and thus tell about the precision of the experimental model. Normal probability plots of residuals and internally studentized residuals plots of residuals *vs* predicted were taken into consideration as presented in Fig. 1. It was found that residuals were distributed along a straight line indicating the normal distribution of error terms. The internally studentized residuals were laid within ± 2 value, indicating the absence of an outlier in the experimental data. These graphs indicated the adequacy of the model.

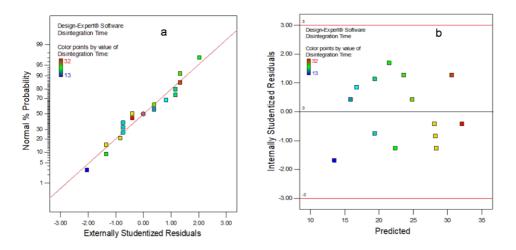


Fig. 1. (a) Normal probability plot of residuals and (b) internally studentized residual plot.

3.9. Effect analysis

The effect of an individual factor on the DT was visualized by one-factor effect graph (Fig. 2). It was found that L-HPC in a concentration around 3 % (w/w) reduced the DT and above 4 % the DT kept rising, indicating increasing binding property at higher

concentration. CCS showed decreasing DT with increasing % w/w concentration and between 4 % to 5 % it reduced the DT at the most and, above 5 % DT kept increasing indicating gel-forming properties of CCS at higher concentration. DT was reduced almost linearly with increasing punch dia.

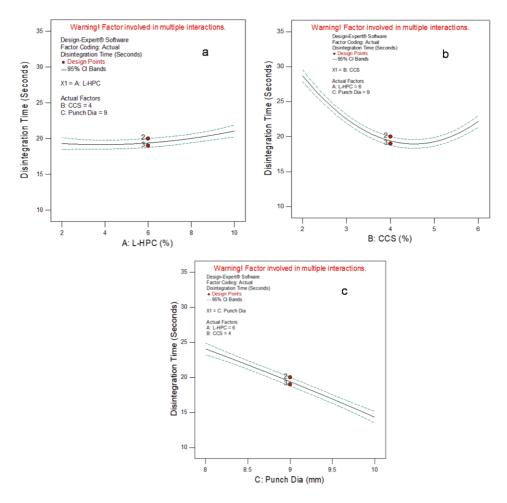


Fig. 2. Effects of (a) L-HPC alone, (b) CCS alone, and (c) punch dia alone on disintegration time.

3.10. Design space

Design space was constructed by overlaid contour plots to visualize the optimum condition for the desired formulation. In creating design space, the target of disintegration was constricted within 20 sec. At first, punch diameter was optimized using design space. It was found that a diameter below 8.6 mm produced no space for target DT regardless of any combination of CCS and L-HPC (Fig. 3). On the other hand, punch dia at 10.0 mm produced a wide space for meeting the target DT. But above 9.5 mm, the thickness of

tablets becomes too low with respect to the tablet weight (220 mg) to handle in the subsequent process (e.g., blistering) and the friability of tablets having a diameter 10.0 mm was found close to a higher limit (1.0 %). Hence, the safe range was selected as 8.7 mm to 9.3 mm while the optimum was considered as 9.0 mm.

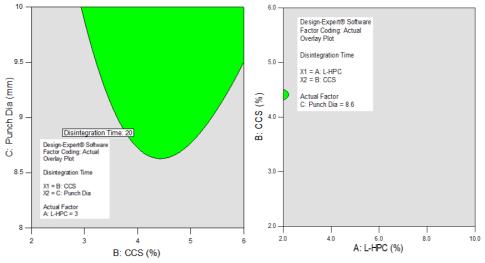


Fig. 3. Finding optimum punch dia in the design space.

Keeping the punch dia at 9.0 mm another overlay contour plot was constructed to create the design space and find the optimum concentration ranges of L-HPC and CCS. The design space was shown in Fig. 4. The green region indicated the design space where each point corresponds to a unique combination of L-HPC and CCS and formulation with any of those combinations meets the target DT. It was, therefore, obvious that within a punch diameter range of 8.7 mm ~ 9.0 mm, L-HPC concentration range of 2 %~8 % w/w and CCS concentration range of 4 % ~ 5 % w/w, the risk of DT was reduced to the lower level as any combination of the factors in those ranges would result a DT of not more than 18 sec. which is much below of the initial target DT of 30 sec.

For the final formulation, % w/w of L-HPC was chosen as 3.0 % and that for CCS was chosen as 4.5 % with a predicted DT of 18.79 sec (with a confidence interval of 18.25 sec~19.33 sec) as shown in the Fig. 4. With this final composition, three small batches were prepared following the same manufacturing procedure and 10 tablets were collected from three stages: initial time of batch start, at the middle of the batch and towards the end of the batch. DT was checked using USP apparatus. Results were presented in Table 8.

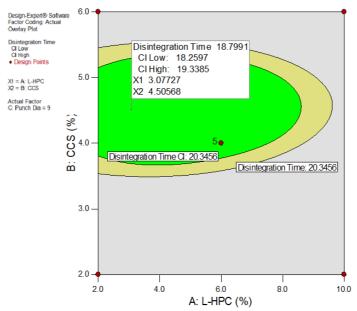


Fig. 4. Overlay contour plot and design space for optimum condition.

Batch No.	DT of 10 tablets from initial stage (Mean±SD)	DT of 10 tablets from middle stage (Mean±SD)	DT of 10 tablets from end stage (Mean±SD)	Mean DT±SEM (sec)
1	18.9±1.37	18.8±1.62	18.2±1.69	18.63±0.28
2	18.1±0.99	18.7±1.42	18.5±1.43	18.43±0.23
3	18±1.33	19.1±1.37	18.9±1.6	18.67±0.26

Table 8. Summary of disintegration time of three batches made following final composition.

3.11. Fine-tuning of final formulation and stability study

The final quantitative composition having been fixed, hardness was optimized. All the optimization batches were compressed within a hardness limit of between $6\sim7$ Kp. Two batches were prepared following the final formula and one was compressed to an average hardness of 5.0 Kp±0.5 Kp and another was of 4.0 Kp±0.5 Kp and friability was checked and found below 1 %. Tablets of the first batch disintegrated within 6 sec ~ 7 sec and tablets of the second batch disintegrated within 5 sec. Tablets from both batches were then packed in aluminum blister and loaded in accelerated stability conditions (40 °C, 75 % relative humidity) and controlled conditions (25 °C, 60 % relative humidity) for the long-term stability study. After 3-months, hardness was found more or less the same as of initial condition in all conditions, but after 6-months, hardness was reduced by 1.0 Kp for the first batch and by 1.5 Kp for second batch on an average. Hardness was found above 3.0 Kp for both batches (data not shown) in controlled condition at 12 months. Hence, the safe hardness limit during manufacturing should consider between 4.0 ~ 7.0 Kp. Assay of ASP was found as low as 92 % at 6 months accelerated condition whereas in controlled

condition assay was found to be ~ 96 % at 12 months. GLY was stable throughout all conditions. Hence, the preferred storage condition is \leq 25 °C in a dry place.

4. Conclusion

In the current study, QTPP and CQA were properly defined and CQAs were examined as a function of those critical formulation attributes and process attributes that were identified as medium to high risk by FMEA risk assessment. Optimization was successfully done through structured experimental design and statistical analysis. A design space was constructed to achieve a robust formula with a low risk for disintegration fail. From the study, it was concluded that an ODT dosage form of aspirin (100 mg) and glycine (45 mg) combination could be formulated in 220 mg round tablet having any diameter between 8.7 ~ 9.3 mm, comprising CCS in a range of 4 % ~ 5 % (w/w), preferably at 4.5 % and L-HPC in a range of 2 % ~ 8 % (w/w), preferably at 3 % and within a hardness range of $4 \sim 7$ Kp for the best oral disintegrating property. Tablets with final composition contain a considerable amount of diluent (201.3 mg of MCC-101), meaning that other compliance agents like flavor/sweetener/ color (which works in minute percentage) can be added to this formulation without hampering the physical properties. In the end, it was an excellent example of QbD based formulation development process as per FDA guidelines for pharmaceutical industries.

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